

Heat Transfer in the flow of a Non-Newtonian second-order fluid over an enclosed torsionally oscillating discs in the presence of the magnetic field

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ABSTRACT: The problem of the heat transfer in the flow of an incompressible non-Newtonian second-order fluid over an enclosed torsionally oscillating discs in the presence of the magnetic field has been discussed. The obtained differential equations are highly non-linear and contain upto fifth order derivatives of the flow and energy functions. Hence exact or numerical solutions of the differential equations are not possible subject to the given natural boundary conditions; therefore the regular perturbation technique is applied. The flow functions H, G, L and M are expanded in the powers of the amplitude ε (taken small) of the oscillations. The behaviour of the temperature distribution at different values of Reynolds number, phase difference, magnetic field and second-order parameters has been studied and shown graphically. The results obtained are compared with those for the infinite torsionally oscillating discs by taking the Reynolds number of out-flow R_m and circulatory flow R_L equals to zero. Nusselt number at oscillating and stator disc has also been calculated and its behaviour is represented graphically.

Keywords: Heat Transfer; Second-Order Fluid; Enclosed Torsionally Oscillating Disc, Magnetic Field.

I. INTRODUCTION

The phenomenon of flow of the fluid over an enclosed torsionally oscillating disc (enclosed in a cylindrical casing) has important engineering applications. The most common practical application of it is the domestic washing machine and blower of curd etc. Soo [1] has considered first the problem of laminar flow over an enclosed rotating disc in case of Newtonian fluid. Sharma and Agarwal [2] have discussed the heat transfer from an enclosed rotating disc in case of Newtonian fluid. Thereafter Singh K. R. and H. G. Sharma [3] have discussed the heat transfer in the flow of a second-order fluid between two enclosed rotating discs. The torsional oscillations of Newtonian fluids have been discussed by Rosenblat [4]. He has also discussed the case when the Newtonian fluid is confined between two infinite torsionally oscillating discs [5]. Sharma & Gupta [6] have considered a general case of flow of a second-order fluid between two infinite torsionally oscillating discs. Thereafter Sharma & K. R. Singh [7] have solved the problem of heat transfer in the flow of a non-Newtonian second-order fluid between torsionally oscillating discs. Hayat [8] has considered non-Newtonian flows over an oscillating plate with variable suction. KR Singh, VK Agrawal & A Singh [9] have discussed Heat transfer in the flow of a non-Newtonian second-order fluid between two enclosed counter torsionally oscillating disc. Chawla [10] has considered flow past of a torsionally oscillating plane Riley & Wybrow [11] have considered the flow induced by the torsional oscillations of an elliptic cylinder. KR Singh, VK Agarwal [12] have solved heat transfer in the flow of a non-Newtonian second-order fluid between two enclosed counter torsionally oscillating discs with uniform suction and injection. Bluckburn [13] has considered a study of two-dimensional flow past of an oscillating cylinder. Sadhna Kahre [14] studied the steady flow between a rotating and porous stationary disc in the presence of transverse magnetic field. Singh & Singhal [15] have discussed flow of a non-Newtonian reiner-rivlin fluid between two enclosed torsionally oscillating porous discs. Agarwal & Agarwal [16] have solved flow of a non-Newtonian second-order fluid over an enclosed torsionally oscillating disc. Agarwal & Agarwal [17] have also discussed flow of a non-Newtonian second-order fluid over an enclosed torsionally oscillating disc in the presence of magnetic field.

Due to complexity of the differential equations and tedious calculations of the solutions, no one has tried to solve the most practical problems of enclosed torsionally oscillating discs so far. The authors have considered the present problem of heat transfer in the flow of a non-Newtonian second-order fluid over an enclosed torsionally oscillating discs in the presence of the magnetic field and calculated successfully the steady and unsteady part both of the flow and energy functions. The flow and energy functions are expanded in the powers of the amplitude ε (assumed to be small) of the oscillations of the disc. The non-Newtonian effects are

exhibited through two dimensionless parameters $\tau_1 \left(= \frac{n\mu_2}{\mu_1} \right)$ and $\tau_2 \left(= \frac{n\mu_3}{\mu_1} \right)$, where μ_1, μ_2, μ_3 are coefficient of Newtonian viscosity, elasto-viscosity and cross-viscosity respectively, n being the uniform frequency of the oscillation. The variation of temperature distribution with elasto-viscous parameter τ_1 , cross-viscous parameter τ_2 (based on the relation $\tau_1 = \alpha\tau_2$ where $\alpha = -0.2$ as for 5.46% poly-iso-butylene type solution in cetane at 30 °C (Markowitz [18]), Reynolds number R , magnetic field 'm' at different phase difference τ is shown graphically.

II. FORMULATION OF THE PROBLEM

The constitutive equation of an incompressible second-order fluid as suggested by Coleman and Noll [19] can be written as:

$$\tau_{ij} = -p\delta_{ij} + 2\mu_1 d_{ij} + 2\mu_2 e_{ij} + 4\mu_3 c_{ij} \quad (1)$$

where

$$d_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i}), e_{ij} = \frac{1}{2}(a_{i,j} + a_{j,i}) + u_i^\alpha u_{\alpha,j} c_{ij} = d_{i\alpha} d_j^\alpha \quad (2)$$

p is the hydrostatic pressure, τ_{ij} is the stress-tensor, d_{ij} is rate of deformation (rate of strain or flow) tensor, u_i and a_i are the velocity and acceleration vector.

The equation (1) together with the momentum equation for no extraneous force

$$\rho \left(\frac{\partial u_i}{\partial x} + u^\alpha u_{i,\alpha} \right) = \tau_{i,\alpha}^\alpha \quad (3)$$

$$\text{and the equation of continuity for incompressible fluid } u_i^i = 0 \quad (4)$$

where ρ is the density of the fluid and comma (,) represents covariant differentiation, form the set of governing equations.

In the three dimensional cylindrical set of co-ordinates (r, θ, z) the system consists of a finite oscillating disc of radius r_s (coinciding with the plane $z = 0$) performing rotatory oscillations of the type $r\Omega \cos t$ of small amplitude ϵ , about the perpendicular axis $r = 0$ with a constant angular velocity Ω in an incompressible second-order fluid forming the part of a cylindrical casing or housing. The top of the casing (coinciding with the plane $z = z_0 < r_s$) may be considered as a stationary disc (stator) placed parallel to and at a distance equal to gap length z_0 from the oscillating disc. The symmetrical radial steady outflow has a small mass rate 'm' of radial outflow ('-m' for net radial inflow). The inlet condition is taken as a simple radial source flow along z-axis starting from radius r_0 . A constant magnetic field B_0 is applied normal to the plane of the oscillating disc. The induced magnetic field is neglected.

Assuming (u, v, w) as the velocity components along the cylindrical system of axes (r, θ, z) the relevant boundary conditions of the problem are:

$$z = 0, \quad u = 0, \quad v = r\Omega e^{it} \text{ (Real part)}, \quad w = 0, \quad T = T_a$$

$$z = z_0, \quad u = 0, \quad v = 0, \quad w = 0, \quad T = T_b \quad (5)$$

where the gap z_0 is assumed small in comparison with the disc radius r_s . The velocity components for the axisymmetric flow compatible with the continuity criterion can be taken as [1],[2],[3].

$$U = -\xi H'(\zeta, \tau) + \left(\frac{R_m}{R_z} \right) \frac{M'(\zeta, \tau)}{\xi}, \quad V = \xi G(\zeta, \tau) + \left(\frac{R_L}{R_z} \right) \frac{L(\zeta, \tau)}{\xi}, \quad W = 2H(\zeta, \tau) \quad (6)$$

and for the temperature, we take

$$T = T_b + \left(\frac{v_1 \Omega}{c_v} \right) \{ \phi(\zeta, \tau) + \zeta^2 \psi(\zeta, \tau) \} \quad (7)$$

Where $U = \frac{u}{\Omega z_0}, V = \frac{v}{\Omega z_0}, W = \frac{w}{\Omega z_0}, \xi = \frac{r}{z_0}, \zeta, \tau$ are dimensionless quantities and $H(\zeta, \tau), G(\zeta, \tau), L(\zeta, \tau), M'(\zeta, \tau), \phi(\zeta, \tau), \Psi(\zeta, \tau)$ are dimensionless function of the dimensionless variables $\zeta = \frac{z}{z_0}$ and $\tau = nt$.

$R_m = \frac{m}{2\pi\rho z_0 v_1}, R_z = \frac{L}{2\pi\rho z_0 v_1}$ are dimensionless number to be called the Reynolds number of net radial outflow and circulatory flow respectively. $R_z \left(= \frac{\Omega z_0^2}{v_1} \right)$ be the flow Reynolds number. The small mass rate 'm' of the radial outflow is represented by $m = 2\pi\rho \int_0^{z_0} r u dz$ (8)

Using expression (6) and (7), the boundary condition (5) transform for $G, L \& H$ into the following form:

$$G(0, \tau) = \text{Real}(e^{it}), G(1, \tau) = 0, L(0, \tau) = 0, L(1, \tau) = 0, H(0, \tau) = 0,$$

$$H(1, \tau) = 0, H'(0, \tau) = 0, H'(1, \tau) = 0, \phi(0, \tau) = \frac{1}{E} = S, \phi(1, \tau) = 0, \Psi(0, \tau) = 0, \Psi(1, \tau) = 0 \quad (9)$$

where $E \left\{ = \frac{\Omega v_1}{c_v(T_a - T_b)} \right\}$ is the Eckert number.

The conditions on M on the boundaries are obtainable form the expression (8) for m as follows:

$$M(1, \tau) - M(0, \tau) = 1 \tag{10}$$

which on choosing the discs as streamlines reduces to

$$M(1, \tau) = 1, M(0, \tau) = 0 \tag{11}$$

Using eqs.(1) and expression (6)in equation (3) and neglecting the squares & higher powers of R_m/R_z (assumed small), we have the following equations in dimensionless form:

$$-\frac{1}{\rho z_0} \frac{\partial p}{\partial \xi} = -n\Omega z_0 \left\{ \xi H' - \left(\frac{R_m}{R_z}\right) \frac{\partial M'}{\xi} \right\} + \Omega^2 z_0 \xi \left(H'^2 - 2HH'' - G^2 \right) + \Omega^2 z_0 \left(\frac{R_m}{R_z}\right) \frac{2HM''}{\xi} - \Omega^2 z_0 \left(\frac{R_L}{R_z}\right) \frac{2LG}{\xi} + \frac{v_1 \Omega}{z_0} \left\{ H''' \xi - \left(\frac{R_m}{R_z}\right) \frac{M'''}{\xi} \right\} - \frac{2v_2}{z_0} \left[\left\{ \frac{n\Omega}{2} \left(\frac{R_m}{R_z}\right) \frac{\partial M'''}{\xi} - \xi H'''' \right\} + \Omega^2 \xi \left(H''^2 - HH'''' \right) + \left(\frac{R_m}{R_z}\right) \frac{\Omega^2}{\xi} \left(H''''M' + H''M'' + H'M'''' + HM'''' - RLRz\Omega^2\xi L'G' + LG'' - 4v_3\Omega^2z_0RmRz12\xi H''M' + H''M'' + H'M'''' - RLRz12\xi 2L'G' + LG'' + \xi 4H''^2 - G'^2 - 2H'H'''' + \sigma B_0^2 \Omega z_0 \rho - \xi H'' + RmRzM'\xi \right) \right] \tag{12}$$

$$0 = -n\Omega z_0 \left\{ \xi \partial G + \left(\frac{R_L}{R_z}\right) \frac{\partial L}{\xi} \right\} - 2\Omega^2 z_0 \xi (HG' - H'G) - \Omega^2 z_0 \left(\frac{R_m}{R_z}\right) \frac{2M'G}{\xi} - \Omega^2 z_0 \left(\frac{R_L}{R_z}\right) \frac{2HL'}{\xi} + \frac{v_1 \Omega}{z_0} \left\{ \xi G'' + RLRzL''\xi + 2v_2z_0n\Omega^2\xi G'' + RLRz\partial L''\xi + RLRz\Omega^2\xi H''L' + H''L'' + HL'''' + H'L'' + \Omega^2\xi HG'' - H''G' + RMRz\Omega^2\xi M'G'' + M''G' + 2v_3\Omega^2z_0\xi H''G'' - H''G' + RLRz1\xi H''L' + H''L'' + H'L'' + RMRz1\xi 2M'G'' + M''G' - \sigma B_0^2 \Omega z_0 \rho \xi G + RLRzL\xi \right\} \tag{13}$$

$$-\left(\frac{1}{\rho z_0}\right) \left(\frac{\partial p}{\partial \xi}\right) = 2n\Omega z_0 \partial H + 4\Omega^2 z_0 HH' - 2v_1 \frac{\Omega H''}{z_0} - \frac{2v_2}{z_0} \left\{ n\Omega \partial H'' + 2\Omega^2 \xi^2 (H''H'''' + G'G'') + \Omega^2 (22H'H'' + 2HH'''' \right\} - \left(\frac{R_M}{R_z}\right) 2\Omega^2 (H''M'''' + H''''M'') + \left(\frac{R_L}{R_z}\right) 2\Omega^2 (L'G'' + L''G') \left\} - \frac{2v_3 \Omega^2}{z_0} \left\{ \xi^2 (H''H'''' + G'G'') + 14H'H'' - \left(\frac{R_M}{R_z}\right) (H''M'''' + H''''M'') + \left(\frac{R_L}{R_z}\right) (L'G'' + L''G') \right\} \tag{14}$$

$$\rho C_v \left(\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial r} + w \frac{\partial T}{\partial z} \right) = K \left\{ \frac{\partial^2 T}{\partial r^2} + \frac{1}{r} \left(\frac{\partial T}{\partial r} \right) + \frac{\partial^2 T}{\partial z^2} \right\} + \Phi \tag{15}$$

Where $\Phi = \tau_j^i a_i^j$ (16)

C_p is the specific heat at constant volume, Φ be the viscous-dissipation function, τ_j^i is the mixed deviatoric stress tensor, K is the thermal conductivity, ρ is the density of the fluid; B_0 and σ are intensity of the magnetic field and conductivity of the fluid considered.

Differentiating (12) w.r.t. ζ and (14) w.r.t. ξ and then eliminating $\partial^2 p / \partial \zeta \partial \xi$ from the equation thus obtained. We get

$$-n\Omega z_0 \left\{ \xi \partial H'' - \left(\frac{R_m}{R_z}\right) \partial M'' / \xi \right\} - 2\Omega^2 z_0 \xi (HH'''' + GG'') + \left(\frac{R_m}{R_z}\right) (2\Omega^2 z_0 / \xi) (H''M'''' + HM'''' - \left(\frac{R_L}{R_z}\right) (2\Omega^2 z_0 / \xi) (LG'' + L'G') - (v_1 \Omega / z_0) \left\{ \left(\frac{R_m}{R_z}\right) (M'''' / \xi) - \xi H'''' \right\} - (2v_2 / z_0) \left[(n\Omega / 2) \left\{ \left(\frac{R_m}{R_z}\right) (\partial M'''' / \xi) - \xi \partial H'''' \right\} - \Omega^2 \xi (2H''H'''' + H''H'''' + HH'''' + 4G'G'') \right] + \left(\frac{R_m}{R_z}\right) (\Omega^2 / \xi) (2H''''M'' + H''M'''' + 2H''M'''' + 2H''M'''' + HM'''' - \left(\frac{R_L}{R_z}\right) (2\Omega^2 / \xi) (2L'G'' + L''G' + LG'''')) - (2v_3 \Omega^2 / z_0) \left\{ \left(\frac{R_m}{R_z}\right) (1/\xi) (H''M'''' + 2H''''M'' + 2H''M'''' + H''M'''' - \left(\frac{R_L}{R_z}\right) (1/\xi) (3L'G'' + 2L''G' + LG'''')) - \xi (H''H'''' + 3G'G'') + 2H''H'''' \right\} + (\sigma B_0^2 \Omega z_0 / \rho) \left\{ -\xi H'' + \left(\frac{R_m}{R_z}\right) (M'' / \xi) \right\} = 0 \tag{17}$$

On equating the coefficients of ξ and $1/\xi$ from the equation (13) & (17), we get the following equations:

$$G'' = R\partial G + 2\epsilon R(HG' - H'G) - \tau_1 \partial G'' - 2\epsilon \tau_1 (HG'''' - H''G'') - 2\epsilon \tau_2 (H'G'' - H''G') + m^2 G \tag{18}$$

$$L'' = R\partial L + 2\epsilon R(M'G + HL') - \tau_1 \partial L'' - 2\epsilon \tau_1 (H''L' + H''''L + HL'''' + H'L'' + 2M'G'' + 2M''G') - 2\epsilon \tau_2 (H''L' + H''''L + H''L'' + 2M'G'' + M''G') + m^2 L \tag{19}$$

$$H^{iv} = R\partial H'' + 2\epsilon R(HH'''' + GG'') - \tau_1 \partial H^{iv} - 2\epsilon \tau_1 (H'H^{iv} + HH'''' + 2H''H'''' + 4G'G'') - 2\epsilon \tau_2 (H'H^{iv} + 2H''H'''' + 3G'G'') + m^2 H'' \tag{20}$$

$$M^{iv} = R\partial M'' + 2\epsilon R(H''M'' + HM'''' - LG'' - L'G') - \tau_1 \partial M^{iv} - 2\epsilon \tau_1 (2H''''M'' + H''M'''' + 2H''M'''' + 2H''M'''' + HM'''' - 4L'G'' - 2L''G' - 2LG'''' - 2\epsilon \tau_2 (H''M'''' + 2H''''M'' + 2H''M'''' + H''M'''' - 3L'G'' - 2L''G' - LG'''')) \tag{21}$$

$$+m^2M'' \quad (21)$$

where $R (=nz_0^2/\nu_1)$ is the Reynolds number, $\tau_1(=nv_2/\nu_1)$, $\tau_2(=nv_3/\nu_1)$ and $\epsilon(=\Omega/n)$ are the dimensionless parameter, $m^2 = \sigma B_0^2 z_0^2/\mu_1$ is the dimensionless magnetic field and $R_m/R_L = \mathbf{m}/\mathbf{L} \approx 1$.

Using (7), (16) in (15) and equating the coefficient of ξ^2 and independent term of ξ^2 , we get $\Psi'' = \epsilon RPr [\partial\Psi/\epsilon - 2H'\Psi + 2H\Psi' - H''\Psi - G'^2 - \tau_1(H''\partial H' + G'\partial G') - 2\epsilon\tau_1(H'H'' + H'G'^2 + HH'' + H''H' + HG'G') - 3\epsilon\tau_2(H'H'' + H'G'^2)]$, (22)

$$4\Psi + \phi'' = \epsilon RPr [\partial\phi/\epsilon + (R_m/R_z)2M'\Psi + 2H\phi' - 12H^2 + (R_m/R_z)2H''M'' - (R_L/R_z)2L'G' - \tau_1\{12H'\partial H' - (R_m/R_z)(H''\partial M'' + M''\partial H'') + (R_L/R_z)(G'\partial L')\}] \quad (23)$$

where $P_r (= \mu_1 C_v/K)$ is the Prandtl number.

III. SOLUTION OF THE PROBLEM

Substituting the expressions

$$G(\zeta, \tau) = \sum \epsilon^N G_N(\zeta, \tau); \quad L(\zeta, \tau) = \sum \epsilon^N L_N(\zeta, \tau); \quad H(\zeta, \tau) = \sum \epsilon^N H_N(\zeta, \tau); \quad M(\zeta, \tau) = \sum \epsilon^N M_N(\zeta, \tau) \quad (24)$$

into (18) to (23) neglecting the terms with coefficient of ϵ^2 (assumed negligible small) and equating the terms independent of ϵ and coefficient of ϵ , we get the following equations:

$$G_0'' = R \partial G_0/\partial \tau - \tau_1 \partial G_0''/\partial \tau + m^2 G_0 \quad (25)$$

$$G_1'' = R \partial G_1/\partial \tau - 2R(H_0'G_0' - H_0G_0'') - \tau_1 \partial G_1''/\partial \tau - 2\tau_1(H_0G_0''' - H_0''G_0') - 2\tau_2(H_0'G_0'' - H_0''G_0') + m^2 G_1(26)$$

$$L_0'' = R \partial L_0/\partial \tau - \tau_1 \partial L_0''/\partial \tau + m^2 L_0 \quad (27)$$

$$L_1'' = R \partial L_1/\partial \tau - 2R(M_0'G_0 + H_0L_0') - \tau_1 \partial L_1''/\partial \tau - 2\tau_1(H_0'''L_0 + H_0''L_0' + H_0'L_0'' + H_0L_0''') + 2M_0''G_0' + 2M_0'G_0'' - 2\tau_2(H_0'''L_0 + H_0''L_0' + H_0'L_0'' + H_0L_0''') + m^2 L_1(28)$$

$$H_0^{iv} = R \partial H_0''/\partial \tau - \tau_1 \partial H_0^{iv}/\partial \tau + m^2 H_0'' \quad (29)$$

$$H_1^{iv} = R \partial H_1''/\partial \tau + 2R(H_0H_0'' + G_0G_0') - \tau_1 \partial H_1^{iv}/\partial \tau - 2\tau_1(H_0'H_0^{iv} + H_0H_0^v + 2H_0''H_0''') + 4G_0'G_0'' - 2\tau_2(3G_0'G_0'' + H_0'H_0^{iv} + 2H_0''H_0''') + m^2 H_1''(30)$$

$$M_0^{iv} = R \partial M_0''/\partial \tau - \tau_1 \partial M_0^{iv}/\partial \tau + m^2 M_0'' \quad (31)$$

$$M_1^{iv} = R \partial M_1''/\partial \tau + 2R(H_0'M_0'' + H_0M_0''') - L_0'G_0 - L_0G_0' - \tau_1 \partial M_1^{iv}/\partial \tau - 2\tau_1(2H_0'''M_0'' + H_0^{iv}M_0' + 2H_0''M_0''') - 4L_0'G_0'' - 2L_0''G_0' - 2L_0G_0''' + H_0M_0^v + 2H_0'M_0^{iv} - 2\tau_2(2H_0'''M_0'' + H_0^{iv}M_0' + 2H_0''M_0''') - 3L_0'G_0'' - 2L_0''G_0' - L_0G_0''' + H_0'M_0^{iv} + m^2 M_1'' \quad (32)$$

$$\Psi_0'' = RP_r \partial \Psi_0, \quad (33)$$

$$\Psi_1'' = RP_r [\partial \Psi_1 - 2H_0'\Psi_0 + 2H_0\Psi_0' - H_0''\Psi_0 - G_0'^2 - \tau_1(H_0''\partial H_0'' + G_0'\partial G_0')], \quad (34)$$

$$4\Psi_0 + \phi_0'' = RP_r \partial \phi_0, \quad (35)$$

$$4\Psi_1 + \phi_1'' = RP_r [\partial \phi_1 + (R_m/R_z)2M_0'\Psi_0 + 2H_0\phi_0' - 12H_0^2 + (R_m/R_z)2H_0''M_0'' - (R_L/R_z)2L_0'G_0' - \tau_1\{12H_0'\partial H_0'' - (R_m/R_z)(H_0''\partial M_0'' + M_0''\partial H_0'') + (R_L/R_z)(G_0'\partial L_0')\}]. \quad (36)$$

Taking $G_n(\zeta, \tau) = G_{ns}(\zeta) + e^{i\tau} G_{nt}(\zeta)$; $L_n(\zeta, \tau) = L_{ns}(\zeta) + e^{i\tau} L_{nt}(\zeta)$

$$H_n(\zeta, \tau) = H_{ns}(\zeta) + e^{2i\tau} H_{nt}(\zeta); \quad M_n(\zeta, \tau) = M_{ns}(\zeta) + e^{2i\tau} M_{nt}(\zeta) \quad (37)$$

Complex notation has been adopted here with the convention that only real parts of the complex quantities have the physical meaning.

Using (19) and (28), the boundary conditions (8) & (10) for $n = 0, 1$ transforms to

$$\begin{aligned} G_{0s}(0) &= 0, & G_{0t}(0) &= 1, & G_{1s}(0) &= 0, & G_{1t}(0) &= 0, & G_{0s}(1) &= 0, & G_{0t}(1) &= 0, & G_{1s}(1) &= 0 \\ &= 0, & G_{1t}(1) &= 0, & H_{0s}(0) &= 0, & H_{0t}(0) &= 0, & H_{1s}(0) &= 0, & H_{1t}(0) &= 0, & H_{0s}(1) &= 0, & H_{0t}(1) &= 0, & H_{1s}(1) &= 0, & H_{1t}(1) &= 0, \\ &= 0, & H_{1t}(1) &= 0, & H_{0s}'(0) &= 0, & H_{0t}'(0) &= 0, & H_{1s}'(0) &= 0, & H_{1t}'(0) &= 0, & H_{0s}'(1) &= 0, & H_{0t}'(1) &= 0, & H_{1s}'(1) &= 0, & H_{1t}'(1) &= 0, \\ L_{0s}(0) &= 0, & L_{0t}(0) &= 0, & L_{1s}(0) &= 0, & L_{1t}(0) &= 0, & L_{0s}(1) &= 0, & L_{0t}(1) &= 0, & L_{1s}(1) &= 0, & L_{1t}(1) &= 0, \\ &= 0, & L_{1t}(1) &= 0, & M_{0s}'(0) &= 0, & M_{0t}'(0) &= 0, & M_{1s}'(0) &= 0, & M_{1t}'(0) &= 0, & M_{0s}'(1) &= 0, & M_{0t}'(1) &= 0, & M_{1s}'(1) &= 0, & M_{1t}'(1) &= 0, \\ &= 0, & M_{1t}(1) &= 0, & M_{0s}(1) &= 1, & M_{0t}(1) &= 0, & M_{1s}(1) &= 0, & M_{1t}(1) &= 0, & M_{0s}(0) &= 0, & M_{0t}(0) &= 0, & M_{1s}(0) &= 0, & M_{1t}(0) &= 0, \\ \Psi_{0s}(0) &= 0, & \Psi_{0t}(0) &= 0, & \Psi_{1s}(0) &= 0, & \Psi_{1t}(0) &= 0, & \Psi_{0s}(1) &= 0, & \Psi_{0t}(1) &= 0, & \Psi_{1s}(1) &= 0, & \Psi_{1t}(1) &= 0, \\ &= 0, & \Psi_{1t}(1) &= 0, & \phi_{0s}(0) &= S, & \phi_{0t}(0) &= 0, & \phi_{1s}(0) &= 0, & \phi_{1t}(0) &= 0, & \phi_{0s}(1) &= 0, & \phi_{0t}(1) &= 0, & \phi_{1s}(1) &= 0, & \phi_{1t}(1) &= 0, \end{aligned} \quad (38)$$

$$G_{0s}(\zeta) = G_{1s}(\zeta) = G_{1t}(\zeta) = 0, \quad G_{0t}(\zeta) = \{1 - (e^f/2 \sinh f)\} e^{f\zeta} + (e^f/2 \sinh f) e^{-f\zeta},$$

where $f = \{(iR + m^2)/(1 + i\tau_1)\}^{1/2} = A + iB$,

where $A = \{[(m^2 + R\tau_1) + \{(m^2 + R\tau_1)^2 + (R - m^2\tau_1)^2\}]/\{2(1 + \tau_1^2)\}\}^{1/2}$,

$B = \{[\{(m^2 + R\tau_1)^2 + (R - m^2\tau_1)^2\} - (m^2 + R\tau_1)]/\{2(1 + \tau_1^2)\}\}^{1/2}$,

$$G_0(\zeta, \tau) = \text{Real}\{e^{i\tau} G_{0t}(\zeta)\} = (A_3 + A_5) \cos \tau - (A_4 + A_6) \sin \tau,$$

where $A_1 = e^A (\cos^2 B \sinh A + \cosh A \sin^2 B) / \{2(\sinh^2 A + \sin^2 B)\}$,

$$A_2 = e^A (\sin B \cos B \sinh A - \cos B \cosh A \sin B) / \{2(\sinh^2 A + \sin^2 B)\},$$

$$A_3 = e^{A\zeta} \{(1 - A_1) \cos B\zeta + A_2 \sin B\zeta\}, \quad A_4 = e^{A\zeta} \{(1 - A_1) \sin B\zeta - A_2 \cos B\zeta\},$$

$$A_5 = e^{-Ac} \{A_1 \cos B\zeta + A_2 \sin B\zeta\}, \quad A_6 = e^{-Ac} \{A_2 \cos B\zeta - A_1 \sin B\zeta\},$$

$$G(\zeta, \tau) = G_0(\zeta, \tau) + \epsilon G_1(\zeta, \tau).$$

$$M_{0s}(\zeta) = C_1 e^{m\zeta}/m^2 + C_2 e^{-m\zeta}/m^2 + C_3 \zeta + C_4, M'_{0s}(\zeta) = C_1 e^{m\zeta}/m - C_2 e^{-m\zeta}/m + C_3,$$

Where $C_1 = C_2(e^m - 1)/(e^m - 1), \quad C_2 = m^2(e^m - 1)/\{4 + e^m(m-2) - e^{-m}(m+2)\}, C_3 = -(C_1 - C_2)/m, C_4 = (C_1 + C_2)/m^2.$

$$M_{0t}(\zeta) = M_{1s}(\zeta) = M_{1t}(\zeta) = 0, \quad M(\zeta, \tau) = M_0(\zeta, \tau) + \epsilon M_1(\zeta, \tau) = M_0(\zeta, \tau).$$

$$H_{0s}(\zeta) = H_{0t}(\zeta) = H_{1s}(\zeta) = 0,$$

$$H_{1t}(\zeta) = C_1 e^{d\zeta}/d^2 + C_2 e^{-d\zeta}/d^2 + C_3 \zeta + C_4 + (Z_1 - f^2 Z_2) \{ [1 - (e^f/2 \sinh f)] \} 2e^{f\zeta}/4f - e^{2f(1-\zeta)}/(16f \sinh^2 f),$$

where $d = \{(2iR + m^2)/(1 + 2i\tau_1)\}^{1/2} = C + iD,$

where $C = \{[(m^2 + 4R\tau_1) + \{(m^2 + 4R\tau_1)^2 + (2R - 2m^2\tau_1)^2\} / \{2(1 + 4\tau_1^2)\}]\}^{1/2},$

$$D = \{[\{(m^2 + 4R\tau_1)^2 + (R - 4m^2\tau_1)^2\} - (2m^2 + 2R\tau_1)] / \{2(1 + 4\tau_1^2)\}\}^{1/2},$$

$$Z_1 = 2R / \{(1 + i\tau_1)(4f^2 - d^2)\}, \quad Z_2 = (8\tau_1 + 6\tau_2) / \{(1 + i\tau_1)(4f^2 - d^2)\}, \quad C_1 = \{d(Z_{10} - Z_9 - Z_6 + Z_5 + C_2 e^{-d})\},$$

$$C_2 = Z_{11} / \{4 - e^{-d}(d+2) + e^d(d-2)\}, \quad C_3 = -\{(C_1/d) - (C_2/d) + Z_5 - Z_6\}, \quad C_4 = -\{(C_1/d^2) + (C_2/d^2) + Z_3 - Z_4\},$$

$$Z_3 = Z_1 \{ [1 - (e^f/2 \sinh f)] \}^2 / 4f - fe^{2f}/16f \sinh^2 f, \quad Z_4 = Z_2 \{ [1 - (e^f/2 \sinh f)] \}^2 / 4f - fe^{2f}/16f \sinh^2 f,$$

$$Z_5 = Z_1 \{ [1 - (e^f/2 \sinh f)] \}^2 / 2 + e^{2f}/8 \sinh^2 f, \quad Z_6 = Z_2 \{ [1 - (e^f/2 \sinh f)] \}^2 / 2 + e^{2f}/8 \sinh^2 f,$$

$$Z_7 = Z_1 \{ [1 - (e^f/2 \sinh f)] \}^2 / 4f - 1/16f \sinh^2 f, \quad Z_8 = Z_2 \{ [1 - (e^f/2 \sinh f)] \}^2 / 4f - 1/16f \sinh^2 f,$$

$$Z_9 = Z_1 \{ [1 - (e^f/2 \sinh f)] \}^2 / 2 + 1/8 \sinh^2 f, \quad Z_{10} = Z_2 \{ [1 - (e^f/2 \sinh f)] \}^2 / 2 + 1/8 \sinh^2 f,$$

$$H_1(\zeta, \tau) = \text{Real}\{e^{2\tau} H_{1t}(\zeta)\} = (A_{81} + A_{89}) \cos 2\tau - (A_{82} + A_{90}) \sin 2\tau,$$

where $A_{13} = 4A^2 - 4B^2 - C^2 + D^2, A_{14} = 8AB - 2CD, A_{15} = 2R(A_{13} - \tau_1 A_{14}) / \{(A_{13} - \tau_1 A_{14})^2 + (\tau_1 A_{13} + A_{14})^2\},$

$$A_{16} = -2R(A_{13} \tau_1 + A_{14}) / \{(A_{13} - \tau_1 A_{14})^2 + (\tau_1 A_{13} + A_{14})^2\}, A_{17} = (8\tau_1 + 6\tau_2)(A_{13} - 2\tau_1 A_{14}) / \{(A_{13} - 2\tau_1 A_{14})^2 + (2\tau_1 A_{13} + A_{14})^2\},$$

$$A_{18} = -(8\tau_1 + 6\tau_2)(2\tau_1 A_{13} + A_{14}) / \{(A_{13} - 2\tau_1 A_{14})^2 + (2\tau_1 A_{13} + A_{14})^2\}, A_{19} = [A\{(1 - A_1)^2 - A_2^2\} + 2BA_2(1 - A_1)] / \{4(A^2 + B^2)\},$$

$$A_{20} = -[B\{(1 - A_1)^2 - A_2^2\} + 2AA_2(1 - A_1)] / \{4(A^2 + B^2)\}, A_{21} = \sinh^2 A \cos^2 B - \cosh^2 A \sin^2 B,$$

$$A_{22} = 2 \sinh A \cos B \cosh A \sin B, A_{23} = e^{2A}(A_{21} \cos 2B + A_{22} \sin 2B) / (A_{21}^2 + A_{22}^2),$$

$$A_{24} = e^{2A}(A_{21} \sin 2B - A_{22} \cos 2B) / (A_{21}^2 + A_{22}^2), A_{25} = (AA_{23} + BA_{24}) / \{16(A^2 + B^2)\}, A_{26} = (AA_{24} - BA_{23}) / \{16(A^2 + B^2)\},$$

$$A_{27} = A_{15}(A_{19} - A_{25}) - A_{16}(A_{20} - A_{26}), \quad A_{28} = A_{16}(A_{19} - A_{25}) + A_{15}(A_{20} - A_{26}), \quad B_1 = (1 - A_1)^2 - A_2^2, \quad B_2 = -2(1 - A_1)A_2,$$

$$X_1 = (A^2 - B^2)(A_{17}A_{27} - A_{18}A_{28}) - 2AB(A_{18}A_{27} + A_{17}A_{28}),$$

$$X_2 = 2AB(A_{17}A_{27} - A_{18}A_{28}) + (A^2 - B^2)(A_{18}A_{27} + A_{17}A_{28}),$$

$$A_{29} = (X_1 A_{15} + X_2 A_{16}) / (A_{15}^2 + A_{16}^2), \quad A_{30} = (X_2 A_{15} - X_1 A_{16}) / (A_{15}^2 + A_{16}^2),$$

$$A_{31} = A_{15} \{ (B_1/2) + (A_{23}/8) \} - A_{16} \{ (B_2/2) + (A_{24}/8) \}, \quad A_{32} = A_{16} \{ (B_1/2) + (A_{23}/8) \} + A_{15} \{ (B_2/2) + (A_{24}/8) \},$$

$$X_3 = (A^2 - B^2)(A_{17}A_{31} - A_{18}A_{32}) - 2AB(A_{18}A_{31} + A_{17}A_{32}), X_4 = 2AB(A_{17}A_{31} - A_{18}A_{32}) + (A^2 - B^2)(A_{18}A_{31} + A_{17}A_{32}),$$

$$A_{33} = (X_3 A_{15} + X_4 A_{16}) / (A_{15}^2 + A_{16}^2), A_{34} = (X_4 A_{15} - X_3 A_{16}) / (A_{15}^2 + A_{16}^2), A_{35} = e^{2A}(A_{19} \cos 2B - A_{20} \sin 2B),$$

$$A_{36} = e^{2A}(A_{20} \cos 2B + A_{19} \sin 2B), \quad A_{37} = (AA_{21} - BA_{22}) / [16\{(AA_{21} - BA_{22})^2 + (BA_{21} + AA_{22})^2\}],$$

$$A_{38} = -(BA_{21} + AA_{22}) / [16\{(AA_{21} - BA_{22})^2 + (BA_{21} + AA_{22})^2\}], \quad A_{39} = A_{15}(A_{35} - A_{37}) - A_{16}(A_{36} - A_{38}),$$

$$A_{40} = A_{16}(A_{35} - A_{37}) + A_{15}(A_{36} - A_{38}), \quad X_5 = (A^2 - B^2)(A_{17}A_{39} - A_{18}A_{40}) - 2AB(A_{18}A_{39} + A_{17}A_{40}),$$

$$X_6 = 2AB(A_{17}A_{39} - A_{18}A_{40}) + (A^2 - B^2)(A_{18}A_{39} + A_{17}A_{40}), \quad A_{41} = (X_5 A_{15} + X_6 A_{16}) / (A_{15}^2 + A_{16}^2),$$

$$A_{42} = (X_6 A_{15} - X_5 A_{16}) / (A_{15}^2 + A_{16}^2), \quad A_{43} = e^{2A}(B_1 \cos 2B - B_2 \sin 2B) / 2, \quad A_{44} = e^{2A}(B_2 \cos 2B + B_1 \sin 2B) / 2,$$

$$A_{45} = A_{21} / \{8(A_{21}^2 + A_{22}^2)\}, \quad A_{46} = -A_{22} / \{8(A_{21}^2 + A_{22}^2)\}, \quad A_{47} = A_{15}(A_{43} + A_{45}) - A_{16}(A_{44} + A_{46}),$$

$$A_{48} = A_{16}(A_{43} + A_{45}) + A_{15}(A_{44} + A_{46}), X_7 = (A^2 - B^2)(A_{17}A_{47} - A_{18}A_{48}) - 2AB(A_{18}A_{47} + A_{17}A_{48}),$$

$$X_8 = 2AB(A_{17}A_{47} - A_{18}A_{48}) + (A^2 - B^2)(A_{18}A_{47} + A_{17}A_{48}), A_{49} = (X_7 A_{15} + X_8 A_{16}) / (A_{15}^2 + A_{16}^2),$$

$$A_{50} = (X_8 A_{15} - X_7 A_{16}) / (A_{15}^2 + A_{16}^2), \quad A_{51} = (C^2 - D^2)(e^C \cos D - 1) - 2CD e^C \sin D,$$

$$A_{52} = 2CD(e^C \cos D - 1) + (C^2 - D^2)e^C \sin D,$$

$$A_{53} = C(e^C \cos D - C - 1) - D(e^C \sin D - D), A_{54} = D(e^C \cos D - C - 1) + C(e^C \sin D - D), A_{55} = A_{27} - A_{29} + A_{31} - A_{33} - A_{39} + A_{41},$$

$$A_{56} = A_{28} - A_{30} + A_{32} - A_{34} - A_{40} + A_{42}, A_{57} = A_{49} - A_{47} - A_{33} + A_{31}, A_{58} = A_{50} - A_{48} - A_{34} + A_{32},$$

$$A_{59} = A_{51}A_{55} - A_{52}A_{56} - A_{53}A_{57} + A_{54}A_{58}, A_{60} = A_{52}A_{55} + A_{51}A_{56} - A_{54}A_{57} - A_{53}A_{58},$$

$$A_{65} = 4 - e^{-C} \{ (C+2) \cos D + D \sin D \} + e^C \{ (C-2) \cos D - D \sin D \},$$

$$A_{66} = -e^{-C} \{ D \cos D - (C+2) \cos D \} + e^C \{ (C-2) \sin D + D \cos D \},$$

$$A_{67} = (A_{59}A_{65} + A_{60}A_{66}) / (A_{65}^2 + A_{66}^2), A_{68} = (A_{60}A_{65} - A_{59}A_{66}) / (A_{65}^2 + A_{66}^2),$$

$$A_{69} = CA_{57} - DA_{58} + A_{67}(e^{-C} \cos D - 1) + A_{68} e^C \sin D, A_{70} = DA_{57} + CA_{58} + A_{68}(e^{-C} \cos D - 1) - A_{67} e^{-C} \sin D,$$

$$A_{71} = \{ A_{69}(e^C \cos D - 1) + A_{70} e^C \sin D \} / \{ (e^C \cos D - 1)^2 + e^{2C} \sin^2 D \},$$

$$A_{72} = \{ A_{70}(e^C \cos D - 1) - A_{69} e^C \sin D \} / \{ (e^C \cos D - 1)^2 + e^{2C} \sin^2 D \},$$

$$A_{73} = -\{ \{ (CA_{71} + DA_{72} - CA_{67} - DA_{68}) / (C^2 + D^2) \} + A_{31} - A_{33} \}, A_{74} = -\{ \{ (CA_{72} - DA_{71} - CA_{68} + DA_{67}) / (C^2 + D^2) \} + A_{32} - A_{34} \},$$

$$A_{75} = \{ A_{71}(C^2 - D^2) + 2CDA_{72} \} / \{ (C^2 - D^2)^2 + 4C^2 D^2 \}, A_{76} = \{ A_{72}(C^2 - D^2) - 2CDA_{71} \} / \{ (C^2 - D^2)^2 + 4C^2 D^2 \},$$

$$A_{77} = \{ A_{67}(C^2 - D^2) + 2CDA_{68} \} / \{ (C^2 - D^2)^2 + 4C^2 D^2 \}, A_{78} = \{ A_{68}(C^2 - D^2) - 2CDA_{67} \} / \{ (C^2 - D^2)^2 + 4C^2 D^2 \},$$

$$A_{79} = -(A_{75} + A_{77} + A_{27} - A_{29}), A_{80} = -(A_{76} + A_{78} + A_{28} - A_{30}),$$

$$A_{81} = e^{C\zeta}(A_{75} \cos D\zeta - A_{76} \sin D\zeta) + e^{-C\zeta}(A_{77} \cos D\zeta + A_{78} \sin D\zeta) + A_{73}\zeta + A_{79},$$

$$A_{82} = e^{C\zeta}(A_{76} \cos D\zeta + A_{75} \sin D\zeta) + e^{-C\zeta}(A_{78} \cos D\zeta - A_{77} \sin D\zeta) + A_{74}\zeta + A_{80},$$

$$A_{83} = A_{15} - (A^2 - B^2)A_{17} + 2ABA_{18}, A_{84} = A_{16} - (A^2 - B^2)A_{18} - 2ABA_{17}, A_{85} = e^{2Ac}(A_{19} \cos 2B\zeta - A_{20} \sin 2B\zeta),$$

$$A_{86} = e^{2Ac}(A_{20} \cos 2B\zeta + A_{19} \sin 2B\zeta), A_{87} = e^{2A(1-\zeta)} \{ A_{37} \cos 2B(1-\zeta) - A_{38} \sin 2B(1-\zeta) \},$$

$$A_{88} = e^{2A(1-\zeta)} \{A_{38} \cos 2B(1-\zeta) + A_{37} \sin 2B(1-\zeta)\},$$

$$A_{89} = A_{83}(A_{85}-A_{87}) - A_{84}(A_{86}-A_{88}), A_{90} = A_{84}(A_{85}-A_{87}) + A_{83}(A_{86}-A_{88}),$$

$$H(\zeta, \tau) = H_0(\zeta, \tau) + \in H_1(\zeta, \tau) = \in H_1(\zeta, \tau)$$

$$L_{0s}(\zeta) = L_{0t}(\zeta) = L_{1s}(\zeta) = 0$$

$$L_{1t}(\zeta) = C_5 e^{\zeta} + C_6 e^{-\zeta} + \{\alpha_3 e^{(m+f)\zeta} + \alpha_7 e^{-(m+f)\zeta}\} / (m^2 + 2mf) + \{\alpha_4 e^{-(m-f)\zeta} + \alpha_6 e^{(m-f)\zeta}\} / (m^2 - 2mf) + (\zeta/2f)(\alpha_5 e^{\zeta} - \alpha_8 e^{-\zeta}) - (\alpha_5 e^{\zeta} + \alpha_8 e^{-\zeta}) / 4f^2,$$

where $C_5 = -[C_6 + \{(\alpha_3 + \alpha_7) / (m^2 + 2mf)\} + \{(\alpha_4 + \alpha_6) / (m^2 - 2mf)\} - \{(\alpha_5 + \alpha_8) / (4f^2)\}]$,

$$C_6 = [[\alpha_3 \{e^{(m+f)} - e^{-f}\} + \{\alpha_7 e^{-(m+f)} - e^{-f}\}] / (m^2 + 2mf) + [\alpha_4 \{e^{-(m-f)} - e^{-f}\} + \{\alpha_6 e^{(m-f)} - e^{-f}\}] / (m^2 - 2mf) + (\alpha_5 e^f - \alpha_8 e^{-f}) / 2f + \alpha_8 \sinh f / 2f^2] / (2 \sinh f),$$

$$\alpha_1 = 1 - (e^f / 2 \sinh f), \quad \alpha_2 = e^f / 2 \sinh f,$$

$$\alpha_3 = \{2RC_1 \alpha_1 / m(1 + I\tau_1)\} - \{4(\tau_1 + \tau_2)C_1 \alpha_1 f / (1 + I\tau_1)\} - \{(4\tau_1 + 2\tau_2)C_1 \alpha_1 f^2 / m(1 + I\tau_1)\},$$

$$\alpha_4 = -\{2RC_2 \alpha_1 / m(1 + I\tau_1)\} - \{4(\tau_1 + \tau_2)C_2 \alpha_1 f / (1 + I\tau_1)\} + \{(4\tau_1 + 2\tau_2)C_2 \alpha_1 f^2 / m(1 + I\tau_1)\},$$

$$\alpha_5 = \{2RC_3 \alpha_1 / (1 + I\tau_1)\} - (4\tau_1 + 2\tau_2)C_2 \alpha_1 f^2 / (1 + I\tau_1),$$

$$\alpha_6 = \{2RC_1 \alpha_2 / m(1 + I\tau_1)\} + \{4(\tau_1 + \tau_2)C_1 \alpha_2 f / (1 + I\tau_1)\} - \{(4\tau_1 + 2\tau_2)C_1 \alpha_2 f^2 / m(1 + I\tau_1)\},$$

$$\alpha_7 = -\{2RC_2 \alpha_2 / m(1 + I\tau_1)\} + \{4(\tau_1 + \tau_2)C_2 \alpha_2 f / (1 + I\tau_1)\} + \{(4\tau_1 + 2\tau_2)C_2 \alpha_2 f^2 / m(1 + I\tau_1)\},$$

$$\alpha_8 = \{2RC_3 \alpha_2 / (1 + I\tau_1)\} - (4\tau_1 + 2\tau_2)C_3 \alpha_2 f^2 / (1 + I\tau_1),$$

$$L_1(\zeta, \tau) = \text{Real}\{e^{i\tau} L_{1t}(\zeta)\} = (B_{47} + B_{51} + B_{55} + B_{59} - B_{63}) \cos \tau - (B_{48} + B_{52} + B_{56} + B_{60} - B_{64}) \sin 2\tau,$$

where $B_3 = 1 / (1 + \tau_1^2), \quad B_4 = -\tau_1 / (1 + \tau_1^2),$

$$B_5 = (2RC_1 / m) \{B_3(1 - A_1) + B_4 A_2\} - 4(\tau_1 + \tau_2)C_1 \{(1 - A_1)(AB_3 - BB_4) + A_2(AB_4 + BB_3)\} - \{(4\tau_1 + 2\tau_2)C_1 / m\} [(A^2 - B^2) \{B_3(1 - A_1) + B_4 A_2\} - 2AB \{B_4(1 - A_1) - B_3 A_2\}],$$

$$B_6 = (2RC_1 / m) \{B_4(1 - A_1) - B_3 A_2\} - 4(\tau_1 + \tau_2)C_1 \{(1 - A_1)(AB_4 + BB_3) + A_2(AB_3 - BB_4)\} - \{(4\tau_1 + 2\tau_2)C_1 / m\} [2AB \{B_3(1 - A_1) + B_4 A_2\} + (A^2 - B^2) \{B_4(1 - A_1) - B_3 A_2\}],$$

$$B_7 = -(2RC_2 / m) \{B_3(1 - A_1) + B_4 A_2\} - 4(\tau_1 + \tau_2)C_2 \{(1 - A_1)(AB_3 - BB_4) + A_2(AB_4 + BB_3)\} + \{(4\tau_1 + 2\tau_2)C_2 / m\} [(A^2 - B^2) \{B_3(1 - A_1) + B_4 A_2\} - 2AB \{B_4(1 - A_1) - B_3 A_2\}],$$

$$B_8 = -(2RC_2 / m) \{B_4(1 - A_1) - B_3 A_2\} - 4(\tau_1 + \tau_2)C_2 \{(1 - A_1)(AB_4 + BB_3) + A_2(AB_3 - BB_4)\} + \{(4\tau_1 + 2\tau_2)C_2 / m\} [2AB \{B_3(1 - A_1) + B_4 A_2\} + (A^2 - B^2) \{B_4(1 - A_1) - B_3 A_2\}],$$

$$B_9 = 2RC_3 \{B_3(1 - A_1) + B_4 A_2\} - (4\tau_1 + 2\tau_2)C_3 [(A^2 - B^2) \{B_3(1 - A_1) + B_4 A_2\} - 2AB \{B_4(1 - A_1) - B_3 A_2\}],$$

$$B_{10} = 2RC_3 \{B_4(1 - A_1) - B_3 A_2\} - (4\tau_1 + 2\tau_2)C_3 [2AB \{B_3(1 - A_1) + B_4 A_2\} + (A^2 - B^2) \{B_4(1 - A_1) - B_3 A_2\}],$$

$$B_{11} = (2RC_1 / m) (B_3 A_1 - B_4 A_2) + 4(\tau_1 + \tau_2)C_1 \{A(B_3 A_1 - B_4 A_2) - B(B_4 A_1 + B_3 A_2)\} - \{(4\tau_1 + 2\tau_2)C_1 / m\} \{(B_3 A_1 - B_4 A_2) (A^2 - B^2) - 2AB(B_4 A_1 + B_3 A_2)\},$$

$$B_{12} = (2RC_1 / m) (B_4 A_1 + B_3 A_2) + 4(\tau_1 + \tau_2)C_1 \{B(B_3 A_1 - B_4 A_2) + A(B_4 A_1 + B_3 A_2)\} - \{(4\tau_1 + 2\tau_2)C_1 / m\} \{(B_3 A_1 - B_4 A_2) 2AB + (A^2 - B^2)(B_4 A_1 + B_3 A_2)\},$$

$$B_{13} = -(2RC_2 / m) (B_3 A_1 - B_4 A_2) + 4(\tau_1 + \tau_2)C_2 \{A(B_3 A_1 - B_4 A_2) - B(B_4 A_1 + B_3 A_2)\} + \{(4\tau_1 + 2\tau_2)C_2 / m\} \{(B_3 A_1 - B_4 A_2) (A^2 - B^2) - 2AB(B_4 A_1 + B_3 A_2)\},$$

$$B_{14} = -(2RC_2 / m) (B_4 A_1 + B_3 A_2) + 4(\tau_1 + \tau_2)C_2 \{B(B_3 A_1 - B_4 A_2) + A(B_4 A_1 + B_3 A_2)\} + \{(4\tau_1 + 2\tau_2)C_2 / m\} \{(B_3 A_1 - B_4 A_2) 2AB + (A^2 - B^2)(B_4 A_1 + B_3 A_2)\},$$

$$B_{15} = 2RC_3 \{B_3 A_1 - B_4 A_2\} - (4\tau_1 + 2\tau_2)C_3 \{(A^2 - B^2)(B_3 A_1 - B_4 A_2) - 2AB(B_4 A_1 + B_3 A_2)\},$$

$$B_{16} = 2RC_3 \{B_4 A_1 + B_3 A_2\} - (4\tau_1 + 2\tau_2)C_3 \{(B_3 A_1 - B_4 A_2) 2AB + (A^2 - B^2)(B_4 A_1 + B_3 A_2)\},$$

$$Y_1 = B_5 \cos B(e^{(m+A)} - e^{-A}) - B_6 \sin B(e^{(m+A)} - e^{-A}), \quad Y_2 = B_6 \cos B(e^{(m+A)} - e^{-A}) + B_5 \sin B(e^{(m+A)} - e^{-A}),$$

$$Y_3 = B_{13} \cos B(e^{-(m+A)} - e^A) + B_{14} \sin B(e^{-(m+A)} - e^A), \quad Y_4 = B_{14} \cos B(e^{-(m+A)} - e^A) - B_{13} \sin B(e^{-(m+A)} - e^A),$$

$$B_{17} = (Y_1 + Y_3), \quad B_{18} = (Y_2 + Y_4), \quad Y_5 = (e^{-(m-A)} - e^A) (B_7 \cos B - B_8 \sin B), \quad Y_6 = (e^{-(m-A)} - e^A) (B_8 \cos B + B_7 \sin B),$$

$$Y_7 = B_{11} \cos B(e^{(m-A)} - e^A) + B_{12} \sin B(e^{(m-A)} - e^A), \quad Y_8 = B_{12} \cos B(e^{(m-A)} - e^A) - B_{11} \sin B(e^{(m-A)} - e^A),$$

$$B_{19} = (Y_5 + Y_7), \quad B_{20} = (Y_6 + Y_8), \quad B_{21} = (m^2 + 2mA) / \{(m^2 + 2mA)^2 + 4m^2 B^2\}, \quad B_{22} = -2mB / \{(m^2 + 2mA)^2 + 4m^2 B^2\},$$

$$B_{23} = (m^2 - 2mA) / \{(m^2 - 2mA)^2 + 4m^2 B^2\}, \quad B_{24} = 2mB / \{(m^2 + 2mA)^2 + 4m^2 B^2\},$$

$$B_{25} = e^A (B_9 \cos B - B_{10} \sin B) - e^{-A} (B_{15} \cos B + B_{16} \sin B), \quad B_{26} = e^A (B_{10} \cos B + B_9 \sin B) - e^{-A} (B_{16} \cos B - B_{15} \sin B),$$

$$B_{27} = (AB_{25} + BB_{26}) / \{2(A^2 + B^2)\}, \quad B_{28} = (AB_{26} - BB_{25}) / \{2(A^2 + B^2)\}, \quad B_{29} = B_{15} \sinh A \cos B - B_{16} \cosh A \sin B,$$

$$B_{30} = B_{16} \sinh A \cos B + B_{15} \cosh A \sin B, \quad B_{31} = \{B_{29}(A^2 - B^2) + 2B_{30} AB\} / \{2\{(A^2 - B^2)^2 + 4A^2 B^2\}\},$$

$$B_{32} = \{B_{30}(A^2 - B^2) - 2B_{29} AB\} / \{2\{(A^2 - B^2)^2 + 4A^2 B^2\}\}, \quad B_{33} = B_{17} B_{21} - B_{18} B_{22}, \quad B_{34} = B_{18} B_{21} + B_{17} B_{22},$$

$$B_{35} = B_{19} B_{23} - B_{20} B_{24}, \quad B_{36} = B_{20} B_{23} + B_{19} B_{24},$$

$$B_{37} = \{(B_{33} + B_{35} + B_{27} + B_{31}) \sinh A \cos B + (B_{34} + B_{36} + B_{28} + B_{32}) \cosh A \sin B\} / 2(\sinh^2 A \cos^2 B + \cosh^2 A \sin^2 B),$$

$$B_{38} = \{(B_{34} + B_{36} + B_{28} + B_{32}) \sinh A \cos B - (B_{33} + B_{35} + B_{27} + B_{31}) \cosh A \sin B\} / \{2(\sinh^2 A \cos^2 B + \cosh^2 A \sin^2 B)\},$$

$$B_{39} = B_{21}(B_5 + B_{13}) - B_{22}(B_6 + B_{14}), \quad B_{40} = B_{22}(B_5 + B_{13}) + B_{21}(B_6 + B_{14}), \quad B_{41} = B_{23}(B_7 + B_{11}) - B_{24}(B_8 + B_{12}),$$

$$B_{42} = B_{24}(B_7 + B_{11}) + B_{23}(B_8 + B_{12}), \quad B_{43} = \{(A^2 - B^2)(B_9 + B_{15}) + 2AB(B_{10} + B_{16})\} / \{4\{(A^2 - B^2)^2 + 4A^2 B^2\}\},$$

$$B_{44} = \{(A^2 - B^2)(B_{10} + B_{16}) - 2AB(B_9 + B_{15})\} / \{4\{(A^2 - B^2)^2 + 4A^2 B^2\}\}, \quad B_{45} = -(B_{37} + B_{39} + B_{41} - B_{43}),$$

$$B_{46} = -(B_{38} + B_{40} + B_{42} - B_{44}), \quad B_{47} = e^{A\zeta} (B_{45} \cos B\zeta - B_{46} \sin B\zeta) + e^{-A\zeta} (B_{37} \cos B\zeta + B_{38} \sin B\zeta),$$

$$B_{48} = e^{A\zeta} (B_{46} \cos B\zeta + B_{45} \sin B\zeta) + e^{-A\zeta} (B_{38} \cos B\zeta - B_{37} \sin B\zeta),$$

$$\begin{aligned}
 B_{49} &= e^{(m+A)\zeta}(B_5\cos B\zeta - B_6\sin B\zeta) + e^{-(m+A)\zeta}(B_{13}\cos B\zeta + B_{14}\sin B\zeta), \\
 B_{50} &= e^{(m+A)\zeta}(B_6\cos B\zeta + B_5\sin B\zeta) + e^{-(m+A)\zeta}(B_{14}\cos B\zeta - B_{13}\sin B\zeta), \\
 B_{51} &= B_{49}B_{21} - B_{50}B_{22}, B_{52} = B_{50}B_{21} + B_{49}B_{22}, B_{53} = e^{-(m+A)\zeta}(B_7\cos B\zeta - B_8\sin B\zeta) + e^{(m+A)\zeta}(B_{11}\cos B\zeta + B_{12}\sin B\zeta), \\
 B_{54} &= e^{-(m+A)\zeta}(B_8\cos B\zeta + B_7\sin B\zeta) + e^{(m+A)\zeta}(B_{12}\cos B\zeta - B_{11}\sin B\zeta), B_{55} = B_{53}B_{23} - B_{54}B_{24}, \\
 B_{56} &= B_{54}B_{23} + B_{53}B_{24}, B_{57} = e^{A\zeta}(B_9\cos B\zeta - B_{10}\sin B\zeta) - e^{-A\zeta}(B_{15}\cos B\zeta + B_{16}\sin B\zeta), \\
 B_{58} &= e^{A\zeta}(B_{10}\cos B\zeta + B_9\sin B\zeta) - e^{-A\zeta}(B_{16}\cos B\zeta - B_{15}\sin B\zeta), B_{59} = \zeta(AB_{57} + BB_{58}) / \{2(A^2 + B^2)\}, \\
 B_{60} &= \zeta(AB_{58} - BB_{57}) / \{2(A^2 + B^2)\}, B_{61} = e^{A\zeta}(B_9\cos B\zeta - B_{10}\sin B\zeta) + e^{-A\zeta}(B_{15}\cos B\zeta + B_{16}\sin B\zeta), \\
 B_{62} &= e^{A\zeta}(B_{10}\cos B\zeta + B_9\sin B\zeta) + e^{-A\zeta}(B_{16}\cos B\zeta - B_{15}\sin B\zeta), B_{63} = \{B_{61}(A^2 - B^2) + 2ABB_{62}\} / [4\{(A^2 - B^2)^2 + 4A^2B^2\}], \\
 B_{64} &= \{B_{62}(A^2 - B^2) - 2ABB_{61}\} / [4\{(A^2 - B^2)^2 + 4A^2B^2\}], \\
 L(\zeta, \tau) &= L_0(\zeta, \tau) + \epsilon L_1(\zeta, \tau) = \epsilon L_1(\zeta, \tau)
 \end{aligned}$$

$$\begin{aligned}
 \Psi_{0s}(\zeta) &= \Psi_{0t}(\zeta) = \Psi_{1s}(\zeta) = 0, \\
 \Psi_{1t}(\zeta) &= C_1 e^{q\zeta} + C_2 e^{-q\zeta} - RP_r f^2(1 + I\tau_1) [\{(\alpha_1^2 e^{2f\zeta} + \alpha_2^2 e^{-2f\zeta}) / (4f^2 - q^2)\} + (2\alpha_1\alpha_2 / q^2)], \\
 \text{where } C_1 &= RP_r f^2(1 + I\tau_1) [\{(\alpha_1^2 + \alpha_2^2) / (4f^2 - q^2)\} + 2\alpha_1\alpha_2 / q^2] - C_2, \\
 C_2 &= \{RP_r f^2(1 + I\tau_1) / 2 \sinh q\} [\{e^q(\alpha_1^2 + \alpha_2^2) - (\alpha_1^2 e^{2f} + \alpha_2^2 e^{-2f}) / (4f^2 - q^2)\} + 2\alpha_1\alpha_2(e^q - 1) / q^2], \\
 q &= (2iRP_r) / 2 = Q(1 + I), \\
 \Psi_1(\zeta, \tau) &= \text{Real}\{e^{2i\tau}\Psi_{1t}(\zeta)\} = (B_{27} - B_{31})\cos 2\tau - (B_{28} - B_{32})\sin 2\tau, \\
 \text{where } X_1 &= e^A(\sinh A \cos^2 B + \cosh A \sin^2 B) / \{2(\sinh^2 A + \sin^2 B)\}, \\
 X_2 &= e^A(\sinh A \cos B \sin B - \cosh A \sin B \cos B) / \{2(\sinh^2 A + \sin^2 B)\}, \quad B_1 = (1 - X_1^2 - X_2^2), \quad B_2 = -2X_2(1 - X_1), \\
 B_3 &= (X_1^2 - X_2^2), \quad B_4 = 2X_1X_2, \quad B_5 = A^2 - B^2 - 2AB\tau_1, \quad B_6 = 2AB + \tau_1(A^2 - B^2), \\
 B_7 &= (B_5 \sinh Q \cos Q + B_6 \cosh Q \sin Q) / (\sinh^2 Q \cos^2 Q + \cosh^2 Q \sin^2 Q), \\
 B_8 &= (B_6 \sinh Q \cos Q - B_5 \cosh Q \sin Q) / (\sinh^2 Q \cos^2 Q + \cosh^2 Q \sin^2 Q), \\
 B_9 &= e^Q \{(B_1 + B_3) \cos Q - (B_2 + B_4) \sin Q\}, \quad B_{10} = e^Q \{(B_1 + B_3) \sin Q + (B_2 + B_4) \cos Q\}, \\
 B_{11} &= \{e^{2A}(B_1 \cos 2B - B_2 \sin 2B) + e^{-2A}(B_3 \cos 2B + B_4 \sin 2B)\}, \\
 B_{12} &= \{e^{2A}(B_2 \cos 2B + B_1 \sin 2B) + e^{-2A}(B_4 \cos 2B - B_3 \sin 2B)\}, \quad B_{13} = (4A^2 - 4B^2) / \{(4A^2 - 4B^2)^2 + (8AB - 2RP_r)^2\}, \\
 B_{14} &= -(8AB - 2RP_r) / \{(4A^2 - 4B^2)^2 + (8AB - 2RP_r)^2\}, \quad B_{15} = B_{13}(B_9 - B_{11}) - B_{14}(B_{10} - B_{12}), \\
 B_{16} &= B_{14}(B_9 B_{11}) + B_{13}(B_{10} - B_{12}), \quad B_{17} = \{X_2(1 - X_1) - X_1 X_2\} / (2RP_r), \quad B_{18} = -\{X_1(1 - X_1) + X_2^2\} / (2RP_r), \\
 B_{19} &= B_{17}(e^Q \cos Q - 1) - B_{18} e^Q \sin Q, \quad B_{20} = B_{18}(e^Q \cos Q - 1) + B_{17} e^Q \sin Q, \quad B_{21} = RP_r \{B_7(B_{15} + 2B_{19}) - \\
 B_8(B_{16} + 2B_{20})\} / 2, \quad B_{22} &= RP_r \{B_8(B_{15} + 2B_{19}) + B_7(B_{16} + 2B_{20})\} / 2, \quad B_{23} = B_{13}(B_1 + B_3) - B_{14}(B_2 + B_4), \\
 B_{24} &= B_{14}(B_1 + B_3) + B_{13}(B_2 + B_4), \\
 B_{25} &= RP_r \{B_5(B_{23} + 2B_{17}) - B_6(B_{24} + 2B_{18})\} - B_{21}, \quad B_{26} = RP_r \{B_6(B_{23} + 2B_{17}) + B_5(B_{24} + 2B_{18})\} - B_{22}, \\
 B_{27} &= e^{Q\zeta}(B_{25} \cos Q\zeta - B_{26} \sin Q\zeta) + e^{-Q\zeta}(B_{21} \cos Q\zeta + B_{22} \sin Q\zeta), \\
 B_{28} &= e^{Q\zeta}(B_{26} \cos Q\zeta + B_{25} \sin Q\zeta) + e^{-Q\zeta}(B_{22} \cos Q\zeta - B_{21} \sin Q\zeta), \\
 B_{29} &= e^{2A\zeta}(B_1 \cos 2B\zeta - B_2 \sin 2B\zeta) + e^{-2A\zeta}(B_3 \cos 2B\zeta + B_4 \sin 2B\zeta), \\
 B_{30} &= e^{2A\zeta}(B_2 \cos 2B\zeta + B_1 \sin 2B\zeta) + e^{-2A\zeta}(B_4 \cos 2B\zeta - B_3 \sin 2B\zeta), \\
 B_{31} &= RP_r \{B_5(B_{29} B_{13} - B_{30} B_{14} + 2B_{17}) - B_6(B_{30} B_{13} + B_{14} B_{29} + 2B_{18})\}, \\
 B_{32} &= RP_r \{B_6(B_{29} B_{13} - B_{30} \\
 B_{14} + 2B_{17}) + B_5(B_{30} B_{13} + B_{14} B_{29} + 2B_{18})\}, \\
 \Psi(\zeta, \tau) &= \Psi_0(\zeta, \tau) + \epsilon \Psi_1(\zeta, \tau) = \epsilon \Psi_1(\zeta, \tau).
 \end{aligned}$$

$$\begin{aligned}
 \phi_{0s}(\zeta) &= S(1 - \zeta), \phi_{0t}(\zeta) = \phi_{1s}(\zeta) = 0, \\
 \phi_{1t}(\zeta) &= C_3 e^{q\zeta} + C_4 e^{-q\zeta} - 2\zeta(C_1 e^{q\zeta} - C_2 e^{-q\zeta}) / q + (C_1 e^{q\zeta} + C_2 e^{-q\zeta}) / q^2 + 4RP_r f^2(1 + I\tau_1) [\{(\alpha_1^2 e^{2f\zeta} + \alpha_2^2 e^{-2f\zeta}) / (4f^2 - q^2)\} - 2\alpha_1\alpha_2 / q^4], \\
 \text{where } C_4 &= -(C_1 e^q - C_2 e^{-q}) / (q \sinh q) - C_2 / q^2 + \{2RP_r f^2(1 + I\tau_1) / \sinh q\} [\{(\alpha_1^2 (e^{2f} - e^q) + \alpha_2^2 (e^{-2f} - e^{-q})) / (4f^2 - q^2)\} + \\
 2\alpha_1\alpha_2(e^q - 1) / q^4], \\
 C_3 &= -[(C_1 + C_2) / q^2 + C_4 + 4RP_r f^2(1 + I\tau_1) [\{(\alpha_1^2 + \alpha_2^2) / (4f^2 - q^2)\} - 2\alpha_1\alpha_2 / q^4]], \\
 \phi_1(\zeta, \tau) &= \text{Real}\{e^{2i\tau}\phi_{1t}(\zeta)\} = B_{67} \cos 2\tau - B_{68} \sin 2\tau, \\
 B_{33} &= \sinh Q \cos Q / (\sinh^2 Q \cos^2 Q + \sin^2 Q \cosh^2 Q), B_{34} = -\sin Q \cosh Q / (\sinh^2 Q \cos^2 Q + \sin^2 Q \cosh^2 Q), \\
 B_{35} &= (B_{33} + B_{34}) / (2Q), \quad B_{36} = (B_{34} - B_{33}) / (2Q), \quad B_{37} = e^Q(B_{25} \cos Q - B_{26} \sin Q) - e^{-Q}(B_{21} \cos Q + B_{22} \sin Q), \\
 B_{38} &= e^Q(B_{26} \cos Q + B_{25} \sin Q) - e^{-Q}(B_{22} \cos Q - B_{21} \sin Q), B_{39} = B_{37} B_{35} - B_{38} B_{36}, \quad B_{40} = B_{38} B_{35} + B_{37} B_{36}, \\
 B_{41} &= (B_{11} - B_9)(B_{13}^2 - B_{14}^2) - 2B_{13} B_{14}(B_{12} - B_{10}), \quad B_{42} = (B_{12} - B_{10})(B_{13}^2 - B_{14}^2) + 2B_{13} B_{14}(B_{11} - B_9), \\
 B_{43} &= 2RP_r \{B_7 \{B_{41} + (B_{20} / (RP_r))\} - B_8 \{B_{42} - (B_{19} / (RP_r))\}\}, \quad B_{44} = 2RP_r \{B_8 \{B_{41} + (B_{20} / (RP_r))\} + B_7 \{B_{42} - (B_{19} / (RP_r))\}\}, \\
 B_{45} &= -B_{39} - \{B_{22} / (2RP_r)\} + B_{43}, \quad B_{46} = -B_{40} + \{B_{21} / (2RP_r)\} + B_{44}, B_{47} = (B_{26} + B_{22}) / (2RP_r), B_{48} = -(B_{25} + B_{21}) / (2RP_r), \\
 B_{49} &= B_{23} B_{13} - B_{24} B_{14} - (B_{18} / RP_r), B_{50} = B_{24} B_{13} + B_{23} B_{14} + (B_{17} / RP_r), B_{51} = 4RP_r (B_5 B_{49} - B_6 B_{50}), \\
 B_{52} &= 4RP_r (B_6 B_{49} + B_5 B_{50}), B_{53} = -(B_{47} + B_{45} + B_{51}), B_{54} = -(B_{48} + B_{46} + B_{52}), \\
 B_{55} &= e^{Q\zeta}(B_{53} \cos Q\zeta - B_{54} \sin Q\zeta) + e^{-Q\zeta}(B_{45} \cos Q\zeta + B_{46} \sin Q\zeta), \\
 B_{56} &= e^{Q\zeta}(B_{54} \cos Q\zeta + B_{53} \sin Q\zeta) + e^{-Q\zeta}(B_{46} \cos Q\zeta - B_{45} \sin Q\zeta), \\
 B_{57} &= e^{Q\zeta}(B_{25} \cos Q\zeta - B_{26} \sin Q\zeta) - e^{-Q\zeta}(B_{21} \cos Q\zeta + B_{22} \sin Q\zeta),
 \end{aligned}$$

$$\begin{aligned}
 B_{58} &= e^{Q\zeta}(B_{26}\cos Q\zeta + B_{25}\sin Q\zeta) - e^{-Q\zeta}(B_{22}\cos Q\zeta - B_{21}\sin Q\zeta), \\
 B_{59} &= \zeta(B_{57} + B_{58})/Q, B_{60} = \zeta(B_{58} - B_{57})/Q, B_{61} = B_{29}(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_{30}, B_{62} = B_{30}(B_{13}^2 - B_{14}^2) + 2B_{13}B_{14}B_{29}, \\
 B_{63} &= B_{61} - (B_{18}/RP_r), B_{64} = B_{62} + (B_{17}/RP_r), B_{65} = 4RP_r(B_5B_{63} - B_6B_{64}), B_{66} = 4RP_r(B_6B_{63} + B_5B_{64}), \\
 B_{67} &= B_{55} - B_{59} + (B_{28}/2RP_r) + B_{65}, B_{68} = B_{56} - B_{60} - (B_{27}/2RP_r) + B_{66}, \\
 \phi(\zeta, \tau) &= \phi_0(\zeta, \tau) + \epsilon\phi_1(\zeta, \tau).
 \end{aligned}$$

Nusselt number at the oscillating and the stator disc are

$$Nu_b = Q_b z_0 / \{K(T_a - T_b)\} = -E[N_4 + \{N_2(\xi^2 - \xi_0^2)/2\}],$$

$$Nu_a = Q_a z_0 / \{K(T_a - T_b)\} = -E[N_3 + \{N_1(\xi^2 - \xi_0^2)/2\}],$$

where $N_1 = Q(Y_{14} - Y_{15} - Y_{16} + Y_{17}) + 2A(Y_{18} - Y_{20}) + 2B(Y_{19} + Y_{21})$,

$$N_2 = Qe^Q \{ \cos Q(Y_{14} - Y_{15}) - \sin Q(Y_{14} + Y_{15}) \} - Qe^{-Q} \{ \cos Q(Y_{16} - Y_{17}) + \sin Q(Y_{16} + Y_{17}) \} + 2e^{2A} \{ \cos 2B(AY_{18} + BY_{19}) - \sin 2B(BY_{18} - AY_{19}) \} - 2e^{-2A} \{ \cos 2B(AY_{20} - BY_{21}) + \sin 2B(BY_{20} + AY_{21}) \},$$

$$N_3 = -S + Q(Y_1 + Y_2 - Y_3 + Y_4) - (Y_5 - Y_7)/Q + 2A(Y_9 - Y_{11}) + 2B(Y_{10} + Y_{12}),$$

$$N_4 = -S + Qe^Q \{ \cos Q(Y_1 + Y_2) + \sin Q(Y_2 - Y_1) \} - Qe^{-Q} \{ \cos Q(Y_3 - Y_4) + \sin Q(Y_3 + Y_4) \} - (e^Q/Q)(Y_5 \cos Q + Y_6 \sin Q) - e^{-Q} \{ \cos Q(Y_5 - Y_6) + \sin Q(Y_5 + Y_6) \} + (e^{-Q}/Q)(Y_7 \cos Q + Y_8 \sin Q) - e^{-Q} \{ \cos Q(Y_7 - Y_8) + \sin Q(Y_7 + Y_8) \} +$$

$$2e^{2A} \{ \cos 2B(AY_9 + BY_{10}) + \sin 2B(AY_{10} - BY_9) \} - 2e^{-2A} \{ \cos 2B(AY_{11} - BY_{12}) + \sin 2B(BY_{11} + AY_{12}) \},$$

$$Y_1 = \{B_{53} + (B_{26})/(2RP_r)\} \in \cos 2\tau - \{B_{54} - (B_{25})/(2RP_r)\} \in \sin 2\tau,$$

$$Y_2 = \{-B_{54} + (B_{25})/(2RP_r)\} \in \cos 2\tau - \{B_{53} + (B_{26})/(2RP_r)\} \in \sin 2\tau,$$

$$Y_3 = \{B_{45} + (B_{22})/(2RP_r)\} \in \cos 2\tau - \{B_{46} - (B_{22})/(2RP_r)\} \in \sin 2\tau,$$

$$Y_4 = \{B_{46} - (B_{21})/(2RP_r)\} \in \cos 2\tau + \{B_{45} + (B_{21})/(2RP_r)\} \in \sin 2\tau,$$

$$Y_5 = (B_{25} + B_{26}) \in \cos 2\tau - (B_{26} - B_{25}) \in \sin 2\tau, Y_6 = (B_{25} - B_{26}) \in \cos 2\tau - (B_{26} + B_{25}) \in \sin 2\tau,$$

$$Y_7 = (B_{21} + B_{22}) \in \cos 2\tau - (B_{22} - B_{21}) \in \sin 2\tau, Y_8 = (B_{22} - B_{21}) \in \cos 2\tau + (B_{21} + B_{22}) \in \sin 2\tau,$$

$$Y_9 = [4RP_r B_5 \{B_1(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_2\} - 4RP_r B_6 \{B_2(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_1\}] \in \cos 2\tau - [4RP_r B_6 \{B_1(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_2\} - 4RP_r B_5 \{B_2(B_{13}^2 - B_{14}^2) + 2B_{13}B_{14}B_1\}] \in \sin 2\tau,$$

$$Y_{10} = [4RP_r B_5 \{-B_2(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_1\} - 4RP_r B_6 \{B_1(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_2\}] \in \cos 2\tau - [4RP_r B_6 \{-B_2(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_1\} + 4RP_r B_5 \{B_1(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_2\}] \in \sin 2\tau,$$

$$Y_{11} = [4RP_r B_5 \{B_3(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_4\} - 4RP_r B_6 \{B_4(B_{13}^2 - B_{14}^2) + 2B_{13}B_{14}B_3\}] \in \cos 2\tau - [4RP_r B_6 \{B_3(B_{13}^2 - B_{14}^2) - 2B_{13}B_{14}B_4\} + 4RP_r B_5 \{B_4(B_{13}^2 - B_{14}^2) + 2B_{13}B_{14}B_3\}] \in \sin 2\tau,$$

$$Y_{12} = [4RP_r B_5 \{B_4(B_{13}^2 - B_{14}^2) + 2B_{13}B_{14}B_3\} - 4RP_r B_6 \{-B_3(B_{13}^2 - B_{14}^2) + 2B_{13}B_{14}B_4\}] \in \cos 2\tau - [4RP_r B_6 \{B_4(B_{13}^2 - B_{14}^2) + 2B_{13}B_{14}B_3\} + 4RP_r B_5 \{-B_3(B_{13}^2 - B_{14}^2) + 2B_{13}B_{14}B_4\}] \in \sin 2\tau,$$

IV. RESULTS AND DISCUSSION

The variation of the dimensionless temperature $(T^* - T_b^*) / (T_a^* - T_b^*)$ with ζ for different values of elasto-viscous parameter $\tau_1 = 1, 4, 11$; when $\xi = 5, \epsilon = 0.02, E = 5, P_r = 4, R = 4, m = 2$ at phase difference $\tau = \pi/3$ and $2\pi/3$ is shown in fig (1) and fig (2) respectively. It is evident from fig (1) that the temperature increases near the lower disc and start decreasing soon rapidly. It is also clear that the dimensionless temperature decreases with an increase in elasto-viscous parameter τ_1 throughout the gap-length. It can be seen from fig (2) that the temperature increases with an increase in elasto-viscous parameter τ_1 near the lower disc and decreases near the upper disc.

The behaviour of the dimensionless temperature $(T^* - T_b^*) / (T_a^* - T_b^*)$ with ζ for different values of Reynolds number $R = 1, 5, 9$; when $\xi = 5, \epsilon = 0.02, E = 5, P_r = 4$, elasto-viscous parameter $\tau_1 = 2, m = 2$ at phase difference $\tau = \pi/3$ and $2\pi/3$ is shown in fig (3) and fig (4) respectively. It can be observed from fig (3) that the temperature is maximum near the lower disc and increases with an increase in Reynolds number whenever it decreases near the upper disc. It is evident from fig (4) that at $R = 1$, the temperature decreases continuously upto $\zeta = 0.7$ approximately and start increasing slowly thereafter. At $R = 5$ and 9 , the temperature decreases near the lower disc first then start increasing and attains its maximum value in the first half of the gap-length. It is also clear that the temperature increases with an increase with an increase in Reynolds number throughout the gap-length.

The variation of the dimensionless temperature $(T^* - T_b^*) / (T_a^* - T_b^*)$ with ζ for different values of magnetic field parameter $m = 1, 3, 5$; when $\xi = 5, \epsilon = 0.02, E = 5, P_r = 4$, elasto-viscous parameter $\tau_1 = 2, R = 4$ at phase difference $\tau = \pi/3$ and $2\pi/3$ is shown in fig (5) and fig (6) respectively. It can be evident from fig (5) that the temperature attains its maximum value in the first half near the lower disc and increases with an increase in magnetic field parameter m . the behaviour of the temperature in fig (6) is reversed to that of fig (5).

The variation of the Nusselt Number Nu_a with ξ for different values of elasto-viscous parameter $\tau_1 = 2, 3, 4$; when $R = 1, E = 5, P_r = 4, \xi_0 = 5, \epsilon = 0.02, m = 2, \tau = \pi/3$ is shown in fig (7). It is clear from this figure

that Nusselt number decreases with ξ throughout the gap-length. It is also seen that Nusselt number increases with an increase in elasto-viscous parameter τ_1 throughout the gap-length.

The variation of the Nusselt Number Nu_b with ξ for different values of elasto-viscous parameter $\tau_1 = 2, 3, 4$; when $R = 1, E = 5, Pr = 4, \xi_0 = 5, \epsilon = 0.02, m = 2, \tau = \pi/3$ is shown in fig (8). It is clear from this figure that Nusselt number increases with ξ throughout the gap-length. It is also seen that Nusselt number decreases with an increase in elasto-viscous parameter τ_1 throughout the gap-length.

The variation of the Nusselt Number Nu_a with ξ for different values of Reynolds number $R = 2, 3, 4$; when $\tau_1 = 2, E = 5, Pr = 4, \xi_0 = 5, \epsilon = 0.02, m = 2, \tau = \pi/3$ is shown in fig (9). It is clear from this figure that Nusselt number decreases with ξ throughout the gap-length. It is also seen that Nusselt number decreases with an increase in Reynolds number R throughout the gap-length.

The variation of the Nusselt Number Nu_b with ξ for different values of Reynolds number $R = 2, 3, 4$; when $\tau_1 = 2, E = 5, Pr = 4, \xi_0 = 5, \epsilon = 0.02, m = 2, \tau = \pi/3$ is shown in fig (10). It is clear from this figure that Nusselt number increases with ξ throughout the gap-length. It is also seen that Nusselt number decreases with an increase in Reynolds number R throughout the gap-length.

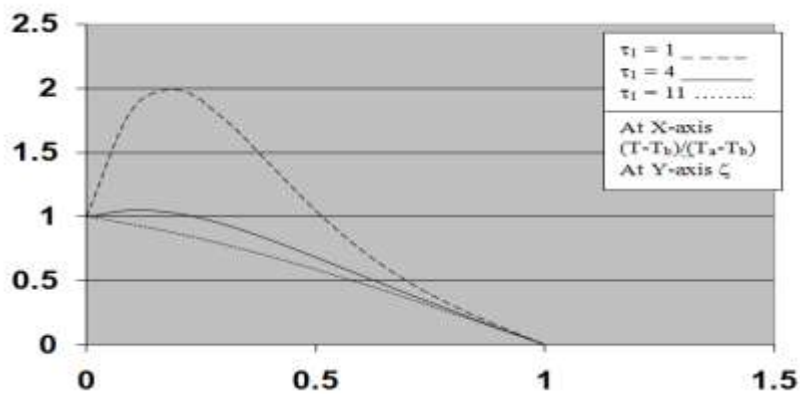
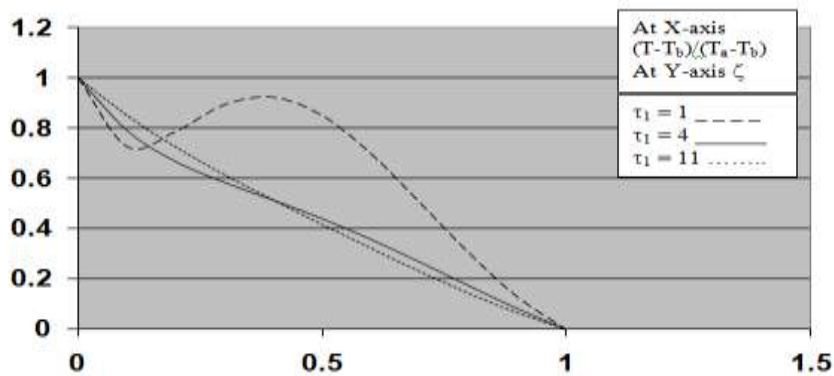
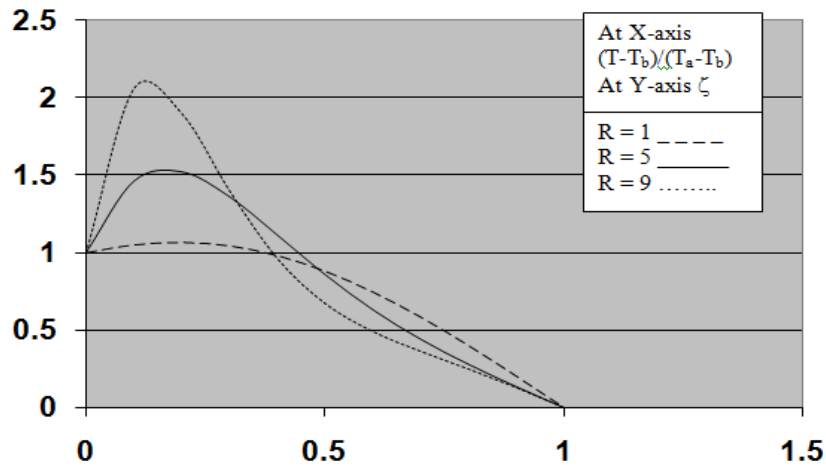


Fig Fig(1) variation of temperature distribution $(T-T_b)/(T_a-T_b)$ at different elasto-viscous parameter τ_1 at $\tau = \pi/3$.

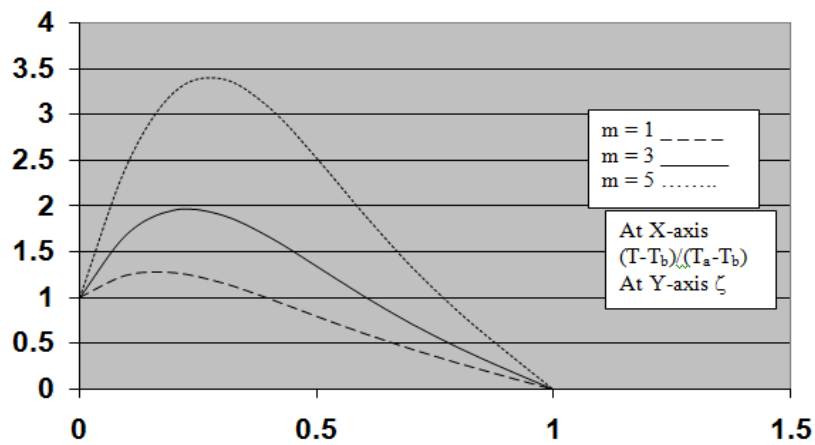


Fig(2) variation of temperature distribution T^* at different elasto-viscous parameter τ_1 at $\tau = 2\pi/3$.

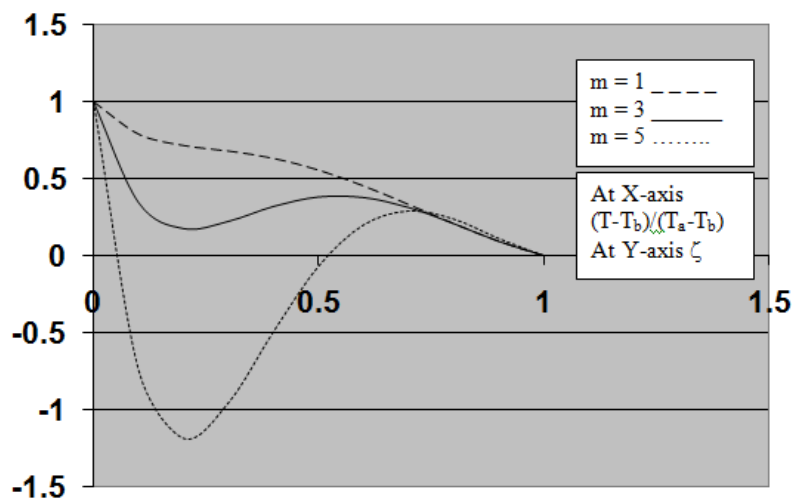
Fig(3) variation of temperature distribution $(T-T_b)/(T_a-T_b)$ at different Reynolds number R at $\tau = \pi/3$.



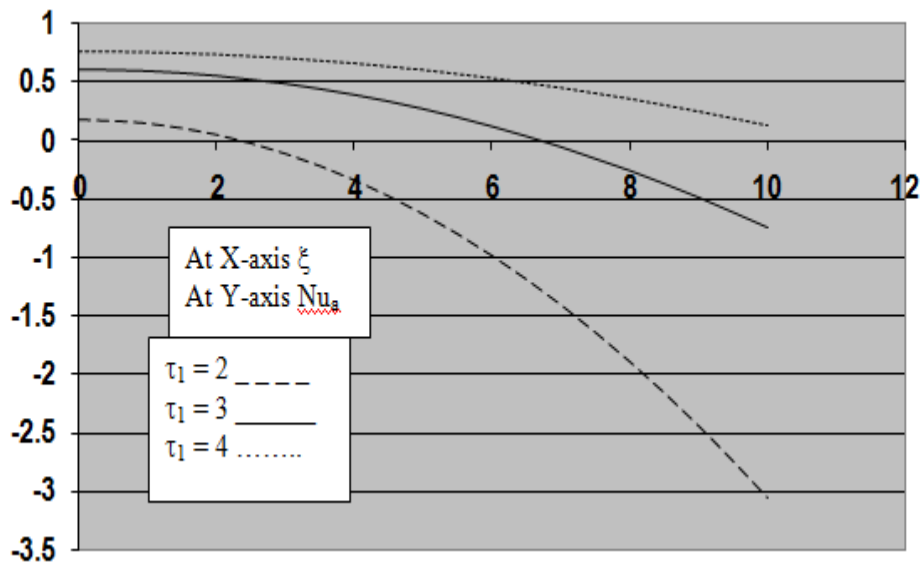
Fig(4) variation of temperature distribution $(T-T_b)/(T_a-T_b)$ at different Reynolds number R at $\tau = 2\pi/3$.



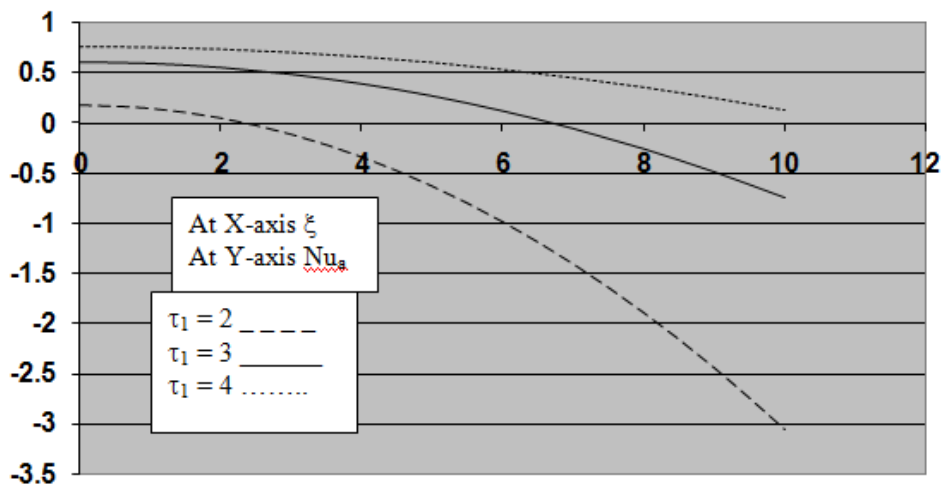
Fig(5) variation of temperature distribution $(T-T_b)/(T_a-T_b)$ at different magnetic field m at $\tau = \pi/3$.



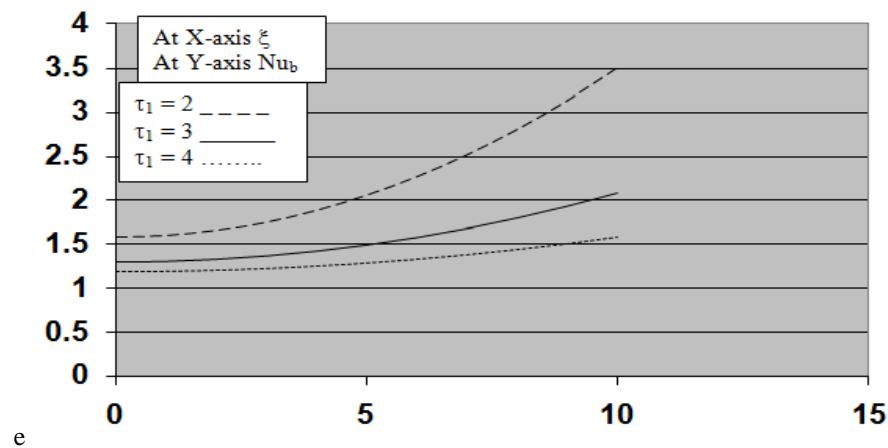
Fig(6) variation of temperature distribution $(T-T_b)/(T_a-T_b)$ at different magnetic field m at $\tau = 2\pi/3$.



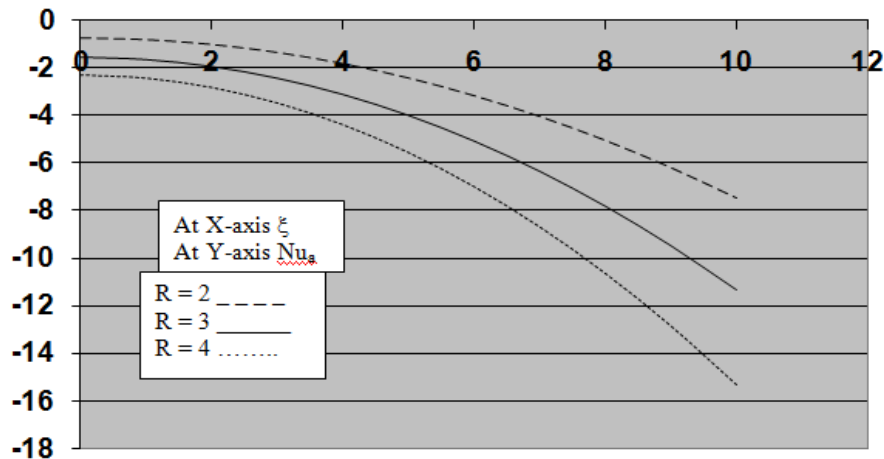
Fig(6) variation of temperature distribution $(T-T_b)/(T_a-T_b)$ at different magnetic field m at $\tau = 2\pi/3$.



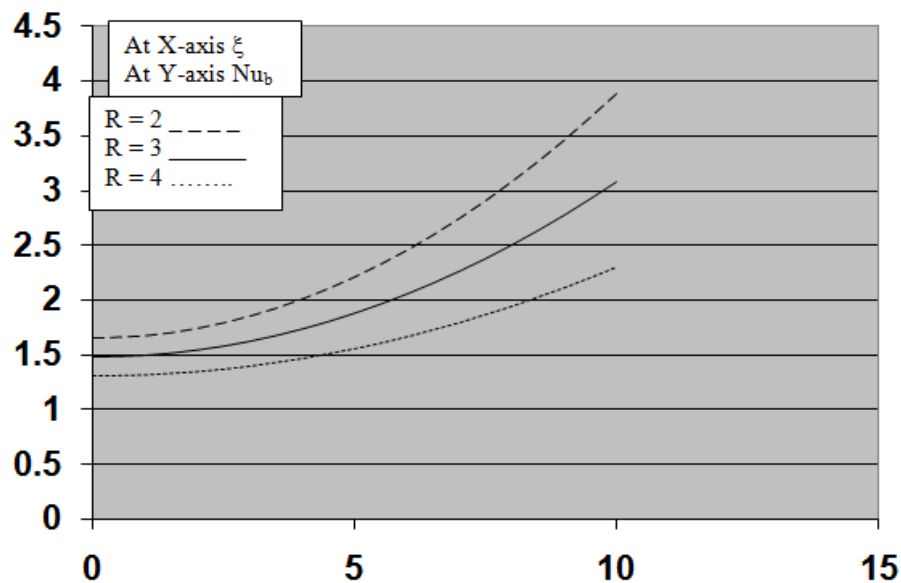
Fig(7) variation of Nusselt number Nu_a at different elasto-viscous parameter τ_1 at $\tau = \pi/3$.



Fig(8) variation of Nusselt number Nu_b at different elasto-viscous parameter τ_1 at $\tau = \pi/3$.



Fig(9) variation of Nusselt number Nu_a at different Reynolds number R at $\tau = \pi/3$.



Fig(10) variation of Nusselt number Nu_b at different Reynolds number R at $\tau = \pi/3$.

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