

Strength of Blended Cement Sandcrete & Soilcrete Blocks Containing Afikpo Rice Husk Ash and Corn Cob Ash

L. O. Ettu,¹ K. C. Nwachukwu,² J. I. Arimanwa,³ T. U. Anyanwu,⁴
S. O. Okpara⁵

^{1,2,3,4}Department of Civil Engineering, Federal University of Technology, Owerri, Nigeria

⁵Department of Building Technology, Akanulbiam Federal Polytechnic, Unwana, Nigeria

Abstract: This work investigated the compressive strength of binary and ternary blended cementsandcrete and soilcreteblocks containing Afikpo rice husk ash (RHA) and corn cob ash (CCA). 135 solid sandcrete blocks and 135 solid soilcrete blocks of 450mm x 225mm x 125mm were produced with OPC-RHAbinary blended cement, 135with OPC-CCAbinary blended cement, and 135with OPC-RHA-CCAternary blended cement, each at percentage OPC replacement with pozzolan of 5%, 10%, 15%, 20%, and 25%.Three sandcrete blocks and three soilcreteblocks for each OPC-pozzolan mix and the control were crushed to obtain their compressive strengths at 3, 7, 14, 21, 28, 50, 90, 120, and 150 days of curing. Binary and ternary blended cement sandcrete and soilcrete block strength values were found to be higher than the control values beyond 50 days of hydration at 5-20% OPC replacement with pozzolan. The 150-day strength values for OPC-RHA-CCA ternary blended cement sandcreteand soilcrete blocks were respectively 6.10N/mm²and 5.30N/mm² for 5% replacement, 6.00N/mm²and 5.20N/mm² for 10% replacement, 5.85N/mm²and 5.00N/mm²for 15% replacement, 5.70N/mm²and 4.95N/mm²for 20% replacement, and 5.35N/mm²and 4.85N/mm²for 25% replacement; while the control values were 5.20N/mm² and 4.80N/mm². Thus, OPC-RHA and OPC-CCA binary blended cements as well as OPC-RHA-CCA ternary blended cement could be used in producing sandcrete and soilcrete blocks with sufficient strength for use in building and minor civil engineering works where the need for high early strength is not a critical factor.

KeyWords: Binary blended cement, corn cob ash, pozzolan, rice husk ash, sandcrete block, soilcrete block, ternary blended cement.

I. Introduction

Sandcrete and soilcrete blocks are cement composites commonly used as walling units in buildings all over South Eastern Nigeria and many other parts of Africa. The major constituents of sandcrete are water, cement, and sand while those of soilcrete are water, cement, and natural soil, especially laterite. These important construction materials have been greatly investigated by many researchers. Mama and Osadebe (2011) developed a mathematical model for optimizing the strength of laterizedsandcrete blocks. Joshua and Lawal (2011) successfully replaced sand with laterite in suitable optimal percentages to produce laterizedsandcrete blocks with adequate strength and more cost effectiveness than the traditional sandcrete blocks. Wenapereand Ephraim (2009) found that the compressive strength of sandcrete blocks increased with age of curing for all mixes tested at the water-cement ratio of 0.5. Their findings showed that the strength at ages 7, 14, and 21 days were 43%, 75%, and 92% of the 28-day strength respectively. Baiden and Tuuli (2004) confirmed that mix ratio, materials quality, and mixing of the constituent materials affect the quality of sandcrete blocks.

Within the past decade researchers in this field have focused largely on finding ways of reducing the cost of cement used in sandcrete and soilcrete block production so as to provide low-cost buildings in the suburbs and villages of South Eastern Nigeria and other places. For this reason agricultural by-products regarded as wastes in technologically underdeveloped societies are increasingly being investigated as partial replacement of Ordinary Portland Cement (OPC) in binary blended cement systems. Manasseh (2010) carried out an elaborate review of some of the commonest agro wastes that have been experimented as cement replacement in sandcrete making and found some of them such as rice husk ash (RHA) suitable. Apata and Alhassan (2012) recently evaluated locally available materials as partial replacement for cement and concluded that partial replacement of these local materials with 10% OPC can be adopted for low cost housing. Okpala (1993) had partially substituted cement with RHA in the percentage range of 30–60% at intervals of 10% while considering the effect on some properties of sandcrete blocks. His results revealed that up to 40% cement replacement would still be suitable for a sandcrete mix of 1:6 (cement/sand ratio) while up to 30%replacement would be suitable for a mix of 1:8. Aribisala and Bamisaye (2006) reported the successful use of bone powder as partial replacement for cement in concrete. Marthong (2012) used sawdust ash (SDA) as partial replacement of cement in sandcrete. Ganesan, Rajagopal, and Thangavel (2008) assessed the optimal level of replacement of OPC with RHA for strength and permeability properties of blended cement concrete. Nair, Jagadish, and Fraaij (2006) found that RHA could be a suitable alternative to OPC for rural housing.

Cisse and Laquerbe (2000) reported that sandcrete blocks obtained with unground Senegalese RHA as partial replacement of OPC had greater mechanical resistance than 100% OPC sandcrete blocks. Their study also revealed that the use of unground RHA enabled production of lightweight sandcrete block with insulating properties at a reduced cost. Agbede and Obam (2008) investigated the strength properties of OPC-RHA blended sandcrete blocks. They replaced various percentages of OPC with RHA and found that up to 17.5% of OPC can be replaced with RHA to produce good quality sandcrete blocks. Oyekan and Kamiyo (2011) reported thatsandcrete blocks made with RHA-blended cement had lower heat

storage capacity and lower thermal mass than 100% OPC sandcrete blocks. They explained that the increased thermal effusivity of the sandcrete block with RHA content is an advantage over 100% OPC sandcrete block as it enhances human thermal comfort. Wada et al. (2000) demonstrated that RHA mortar and concrete exhibited higher compressive strength than the control mortar and concrete. Mehta and Pirtz (2000) investigated the use of rice husk ash to reduce temperature in high strength mass concrete and concluded that RHA is very effective in reducing the temperature of mass concrete compared to OPC concrete. Sakr (2006) investigated the effects of silica fume and rice husk ash on the properties of heavy weight concrete and found that these pozzolans gave higher concrete strengths than OPC concrete at curing ages of 28 days and above. Malhotra and Mehta (2004) reported that ground RHA with finer particle size than OPC improves concrete properties as higher substitution amounts result in lower water absorption values and the addition of RHA causes an increment in the compressive strength. Cordeiro, Filho, and Fairbairn (2009) investigated Brazilian RHA and rice straw ash (RSA) and demonstrated that grinding increased the pozzolanicity of RHA and that high strength of RHA, RSA concrete makes production of blocks with good bearing strength in a rural setting possible. Their study showed that combination of RHA or RSA with lime produces a weak cementitious material which could however be used to stabilize laterite and improve the bearing strength of the material. Rukzon, Chindaprasirt, and Mahachai (2009) studied the effect of grinding on the chemical and physical properties of rice husk ash and the effects of RHA fineness on properties of mortar and found that pozzolans with finer particles had greater pozzolanic reaction. Habeeb and Fayyadh (2009) also investigated the influence of RHA average particle size on the properties of concrete and found that at early ages the strength was comparable, while at the age of 28 days finer RHA exhibited higher strength than the sample with coarser RHA. Cordeiro, Filho, and Fairbairn (2009) further investigated the influence of different grinding times on the particle size distribution and pozzolanic activity of RHA obtained by uncontrolled combustion in order to improve the performance of the RHA. The study revealed the possibility of using ultrafine residual RHA containing high-carbon content in high-performance concrete.

Some researchers have also investigated the possibility of ternary blended cement systems whereby OPC is blended with two different pozzolans. The ternary blended system has two additional environmental and economic advantages. First, it enables a further reduction of the quantity of OPC in blended cements. Second, it makes it possible for two pozzolans to be combined with OPC even if neither of them is available in very large quantity. Fri'as et al. (2005) studied the influence of calcining temperature as well as clay content in the pozzolanic activity of sugar cane straw-clay ashes-lime systems. All calcined samples showed very high pozzolanic activity and the fixation rate of lime varied with calcining temperature and clay content. Elinwa, Ejeh, and Akpabio (2005) investigated the use of sawdust ash in combination with metakaolin as a ternary blend with 3% added to act as an admixture in concrete. Tyagher, Utsev, and Adagba (2011) found that sawdust ash-lime mixture as partial replacement for OPC is suitable for the production of sandcrete hollow blocks. They reported that 10% replacement of OPC with SDA-lime gave the maximum strength at water-cement ratio of 0.55 for 1:8 mix ratio. Fadzil et al. (2008) studied the properties of ternary blended cementitious (TBC) systems containing OPC, ground Malaysian RHA, and fly ash (FA). They found that compressive strength of concrete containing TBC gave low strength at early ages, even lower than that of OPC, but higher than binary blended cementitious (BBC) concrete containing FA. Their results suggested the possibility of using TBC systems in the concrete construction industry and that TBC systems could be particularly useful in reducing the volume of OPC used. Rukzon and Chindaprasirt (2006) investigated the strength development of mortars made with ternary blends of OPC, ground RHA, and classified fly ash (FA). The results showed that the strength at the age of 28 and 90 days of the binary blended cement mortar containing 10 and 20% RHA were slightly higher than those of the control, but less than those of FA. Ternary blended cement mixes with 70% OPC and 30% of combined FA and RHA produced strengths similar to that of the control. The researchers concluded that 30% of OPC could be replaced with the combined FA and RHA pozzolans without significantly lowering the strength of the mixes.

Most of the previous researches on ternary blended cements were based on the ternary blending of OPC with an industrial by-product pozzolan such as FA or silica fume (SF) and an agricultural by-product pozzolan, especially RHA. Tons of agricultural wastes such as rice husk and corn cob are generated in Afikpo district and some other communities in South Eastern Nigeria due to intensified food production and local economic ventures. Not much has been reported on the possibility of binary combination of these Nigerian agricultural by-products with OPC in developing blended cements and no literature exists on the possibility of ternary blending of two of them with OPC. This work is part of a pioneer investigation of the suitability of using two Nigerian agricultural by-products in ternary blend with OPC for sandcrete and soilcrete block making. The compressive strength of binary and ternary blended cements sandcrete and soilcrete blocks containing Afikpo rice husk ash and corn cob ash was specifically investigated. It is hoped that the successful utilization of Afikpo rice husk ash and corn cob ash in binary and ternary combination with OPC for making sandcrete and soilcrete blocks would help in reducing the cost of building and minor civil engineering projects that make much use of sandcrete and soilcrete blocks as well as add economic value to these wastes.

II. Methodology

Rice husk was obtained from rice milling factories in Afikpo district of Ebonyi State and corn cob from Aba district in Abia State, both in South East Nigeria. These materials were air-dried, pulverized into smaller particles, and calcined into ashes in a locally fabricated furnace at temperatures generally below 650°C. The rice husk ash (RHA) and corn cob ash (CCA) were sieved and large particles retained on the 600µm sieve were discarded while those passing the sieve were used for this work. No grinding or any special treatment to improve the quality of the ashes and enhance their pozzolanicity was applied. The RHA had a bulk density of 760 Kg/m³, specific gravity of 1.81, and fineness modulus of 1.40. The CCA had a bulk density of 800 Kg/m³, specific gravity of 1.90, and fineness modulus of 2.02. Other materials used for this work are

Ibeto brand of Ordinary Portland Cement (OPC) with a bulk density of 1650 Kg/m³ and specific gravity of 3.13; river sand free from debris and organic materials with a bulk density of 1590 Kg/m³, specific gravity of 2.68, and fineness modulus of 2.82; laterite also free from debris and organic materials with a bulk density of 1450 Kg/m³, specific gravity of 2.30, and fineness modulus of 3.30; and water free from organic impurities.

A simple form of pozzolanicity test was carried out for each of the ashes. It consists of mixing a given mass of the ash with a given volume of Calcium hydroxide solution [Ca(OH)₂] of known concentration and titrating samples of the mixture against H₂SO₄ solution of known concentration at time intervals of 30, 60, 90, and 120 minutes using Methyl Orange as indicator at normal temperature. For each of the ashes the titre value was observed to reduce with time, confirming the ash as a pozzolan that fixed more and more of the calcium hydroxide, thereby reducing the alkalinity of the mixture.

A standard mix ratio of 1:6 (blended cement: sand (or laterite)) was used for both the sandcrete and the soilcrete blocks. Batching was by weight and a constant water/cement ratio of 0.6 was used. Mixing was done manually on a smooth concrete pavement. For binary blending with OPC, each of the ashes was first thoroughly blended with OPC at the required proportion and the homogenous blend was then mixed with the sand in the case of sandcrete blocks and with laterite in the case of soilcrete blocks, also at the required proportions. For ternary blending, the two ashes were first blended in equal proportions and subsequently blended with OPC at the required proportions before mixing with the sand or laterite, also at the required proportions. Water was then added gradually and the entire sandcrete or soilcrete heap was mixed thoroughly to ensure homogeneity.

One hundred and thirty-five (135) solid sandcrete blocks and one hundred and thirty-five (135) solid soilcrete blocks of 450mm x 225mm x 125mm were produced with OPC-RHAbinary blended cement, one hundred and thirty-five (135) with OPC-CCAbinary blended cement, and one hundred and thirty-five (135) with OPC-RHA-CCA ternary blended cement, each at percentage OPC replacement with pozzolan of 5%, 10%, 15%, 20%, and 25%. Twenty seven (27) sandcrete blocks and twenty seven (27) soilcrete blocks were also produced with 100% OPC or 0% replacement with pozzolan to serve as control. This gives a total of 432 sandcrete blocks and 432 soilcrete blocks. All the blocks were cured by water sprinkling twice a day in a shed. Three sandcrete blocks and three soilcrete blocks for each OPC-pozzolan mix and the control were tested for saturated surface dry bulk density and crushed to obtain their compressive strengths at 3, 7, 14, 21, 28, 50, 90, 120, and 150 days of curing.

III. Results and Discussion

The pozzolanicity test confirmed both the RHA and the CCA as pozzolans since they fixed some quantities of lime over time. The particle size analysis showed that both ashes were much coarser than OPC, the reason being that they were not ground to finer particles. This implies that the compressive strength values obtained using them could still be improved upon if the ashes are ground to finer particles. The compressive strengths of the OPC-RHA and OPC-CCA binary blended cement sandcrete and soilcrete blocks as well as the OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks are shown in tables 1, 2, and 3 for 3-14 days, 21-50 days, and 90-150 days of curing respectively.

Tables 1, 2, and 3 show that the strength values for OPC-RHA and OPC-CCA binary blended cement sandcrete and soilcrete blocks as well as those of OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks were all less than the equivalent control values at 3-28 days of hydration for all percentage replacements of OPC with pozzolans. The strength values of the binary and ternary blended cement sandcrete and soilcrete blocks were the same with the equivalent control values at about 50 days of hydration and greater than the control values at curing ages beyond 50 days. The 150-day strength values for OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks were respectively 6.10N/mm² and 5.30N/mm² for 5% replacement, 6.00N/mm² and 5.20N/mm² for 10% replacement, 5.85N/mm² and 5.00N/mm² for 15% replacement, 5.70N/mm² and 4.95N/mm² for 20% replacement, and 5.35N/mm² and 4.85N/mm² for 25% replacement; while the control values were 5.20N/mm² and 4.80N/mm². The lower strength values of blended cement sandcrete and soilcrete blocks at earlier days of hydration show that pozzolanic reaction was not yet much at those earlier periods; the pozzolanic reaction became higher at later curing ages and this accounts for the much increase in strength of blended cement sandcrete and soilcrete blocks compared to the control specimens.

Table 1. Compressive strength of blended OPC-RHA-CCA cement sandcrete and soilcrete blocks at 3-14 days of curing

| OPC Plus | Compressive Strength of sandcrete blocks (N/mm ²) | | | | | | Compressive Strength of soilcrete blocks (N/mm ²) | | | | | |
|---------------------------|---|---------|----------|----------|----------|----------|---|---------|----------|----------|----------|----------|
| | 0% Poz. | 5% Poz. | 10% Poz. | 15% Poz. | 20% Poz. | 25% Poz. | 0% Poz. | 5% Poz. | 10% Poz. | 15% Poz. | 20% Poz. | 25% Poz. |
| | Strength at 3 days | | | | | | | | | | | |
| RHA | 0.90 | 0.70 | 0.60 | 0.55 | 0.50 | 0.45 | 0.80 | 0.60 | 0.50 | 0.45 | 0.35 | 0.30 |
| CCA | 0.90 | 0.65 | 0.60 | 0.50 | 0.45 | 0.40 | 0.80 | 0.55 | 0.50 | 0.40 | 0.35 | 0.30 |
| RHA & CCA | 0.90 | 0.65 | 0.60 | 0.50 | 0.50 | 0.40 | 0.80 | 0.60 | 0.55 | 0.45 | 0.35 | 0.30 |
| Strength at 7 days | | | | | | | | | | | | |
| RHA | 1.50 | 1.30 | 1.20 | 1.15 | 1.00 | 0.90 | 1.30 | 1.10 | 1.00 | 0.90 | 0.80 | 0.65 |

| | | | | | | | | | | | | |
|----------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| CCA | 1.50 | 1.25 | 1.20 | 1.10 | 0.95 | 0.90 | 1.30 | 1.05 | 1.00 | 0.80 | 0.75 | 0.60 |
| RHA & CCA | 1.50 | 1.25 | 1.20 | 1.10 | 1.00 | 0.90 | 1.30 | 1.10 | 1.00 | 0.85 | 0.80 | 0.60 |
| Strength at 14 days | | | | | | | | | | | | |
| RHA | 2.70 | 2.40 | 2.30 | 2.20 | 2.05 | 1.90 | 2.30 | 2.00 | 1.90 | 1.80 | 1.65 | 1.50 |
| CCA | 2.70 | 2.35 | 2.25 | 2.10 | 2.00 | 1.90 | 2.30 | 1.90 | 1.80 | 1.75 | 1.60 | 1.50 |
| RHA & CCA | 2.70 | 2.35 | 2.25 | 2.15 | 2.00 | 1.90 | 2.30 | 1.95 | 1.90 | 1.75 | 1.60 | 1.55 |

Table 2. Compressive strength of blended OPC-RHA-CCA cement sandcrete and soilcreteblocks at 21-50 days of curing

| OPC Plus | Compressive Strength of sandcrete blocks (N/mm ²) | | | | | | Compressive Strength of soilcrete blocks (N/mm ²) | | | | | |
|----------------------------|---|---------|----------|----------|----------|----------|---|---------|----------|----------|----------|----------|
| | 0% Poz. | 5% Poz. | 10% Poz. | 15% Poz. | 20% Poz. | 25% Poz. | 0% Poz. | 5% Poz. | 10% Poz. | 15% Poz. | 20% Poz. | 25% Poz. |
| | Strength at 21 days | | | | | | | | | | | |
| RHA | 3.50 | 3.25 | 3.15 | 3.10 | 3.00 | 2.80 | 3.10 | 2.80 | 2.70 | 2.60 | 2.55 | 2.40 |
| CCA | 3.50 | 3.15 | 3.05 | 3.00 | 2.90 | 2.70 | 3.10 | 2.70 | 2.65 | 2.50 | 2.40 | 2.30 |
| RHA & CCA | 3.50 | 3.20 | 3.10 | 3.00 | 2.90 | 2.75 | 3.10 | 2.70 | 2.65 | 2.50 | 2.45 | 2.30 |
| Strength at 28 days | | | | | | | | | | | | |
| RHA | 4.40 | 4.20 | 4.10 | 4.05 | 3.90 | 3.75 | 3.90 | 3.70 | 3.55 | 3.50 | 3.40 | 3.30 |
| CCA | 4.40 | 4.10 | 3.90 | 3.80 | 3.75 | 3.60 | 3.90 | 3.50 | 3.45 | 3.35 | 3.30 | 3.25 |
| RHA & CCA | 4.40 | 4.10 | 3.90 | 3.90 | 3.85 | 3.65 | 3.90 | 3.60 | 3.50 | 3.40 | 3.35 | 3.25 |
| Strength at 50 days | | | | | | | | | | | | |
| RHA | 4.70 | 4.70 | 4.60 | 4.55 | 4.50 | 4.30 | 4.30 | 4.50 | 4.45 | 4.30 | 4.10 | 4.00 |
| CCA | 4.70 | 4.60 | 4.50 | 4.40 | 4.35 | 4.20 | 4.30 | 4.40 | 4.30 | 4.25 | 4.05 | 3.95 |
| RHA & CCA | 4.70 | 4.60 | 4.55 | 4.40 | 4.40 | 4.30 | 4.30 | 4.40 | 4.30 | 4.25 | 4.10 | 4.00 |

Table 3. Compressive strength of blended OPC-RHA-CCA cement sandcrete and soilcreteblocks at 90-150 days of curing

| OPC Plus | Compressive Strength of sandcrete blocks (N/mm ²) | | | | | | Compressive Strength of soilcrete blocks (N/mm ²) | | | | | |
|-----------------------------|---|---------|----------|----------|----------|----------|---|---------|----------|----------|----------|----------|
| | 0% Poz. | 5% Poz. | 10% Poz. | 15% Poz. | 20% Poz. | 25% Poz. | 0% Poz. | 5% Poz. | 10% Poz. | 15% Poz. | 20% Poz. | 25% Poz. |
| | Strength at 90 days | | | | | | | | | | | |
| RHA | 4.90 | 5.25 | 5.10 | 5.00 | 4.90 | 4.80 | 4.50 | 4.90 | 4.80 | 4.65 | 4.60 | 4.45 |
| CCA | 4.90 | 5.10 | 5.00 | 4.90 | 4.80 | 4.65 | 4.50 | 4.85 | 4.75 | 4.60 | 4.55 | 4.30 |
| RHA & CCA | 4.90 | 5.20 | 5.10 | 4.90 | 4.85 | 4.70 | 4.50 | 4.90 | 4.75 | 4.60 | 4.55 | 4.30 |
| Strength at 120 days | | | | | | | | | | | | |
| RHA | 5.10 | 5.95 | 5.70 | 5.60 | 5.45 | 5.25 | 4.70 | 5.30 | 5.10 | 5.00 | 4.95 | 4.80 |
| CCA | 5.10 | 5.80 | 5.60 | 5.50 | 5.40 | 5.15 | 4.70 | 5.10 | 5.00 | 4.95 | 4.80 | 4.65 |
| RHA & CCA | 5.10 | 5.90 | 5.60 | 5.50 | 5.40 | 5.20 | 4.70 | 5.20 | 5.00 | 5.00 | 4.85 | 4.70 |
| Strength at 150 days | | | | | | | | | | | | |
| RHA | 5.20 | 6.25 | 6.10 | 5.90 | 5.75 | 5.45 | 4.80 | 5.50 | 5.30 | 5.10 | 5.00 | 4.90 |
| CCA | 5.20 | 6.00 | 5.90 | 5.80 | 5.70 | 5.30 | 4.80 | 5.25 | 5.15 | 5.00 | 4.90 | 4.85 |
| RHA & CCA | 5.20 | 6.10 | 6.00 | 5.85 | 5.70 | 5.35 | 4.80 | 5.30 | 5.20 | 5.00 | 4.95 | 4.85 |

It can also be seen from tables 1-3 that the strength values of OPC-RHA binary blended cement sandcrete and soilcrete blocks were consistently greater than those of OPC-CCA binary blended cement sandcrete and soilcrete blocks for all percentage replacements of OPC with pozzolans at all curing ages. This shows that RHA has a higher pozzolanic reactivity than CCA. The strength of the OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks was consistently in-between the values of the OPC-RHA and OPC-CCA binary blended cement sandcrete and soilcrete blocks. Therefore, more RHA than CCA should be utilized if the two pozzolans are to be used in unequal proportions to optimize the strength of the OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks. However, the closeness in strength values of OPC-RHA and OPC-CCA binary blended cement sandcrete and soilcrete blocks and the fact that the strength of the OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks was in-between these values suggests that the two agricultural by-product pozzolans could be combined in any available proportions individually in binary blending or together in ternary blending with OPC in making blended cement sandcrete and soilcrete blocks.

The results in tables 1 to 3 further show that the values of soilcrete block strength are consistently less than the corresponding values of sandcrete block strength for all percentages of OPC replacement with pozzolans and at all curing ages. This confirms that sand is better than laterite as fine aggregate material in making cement composites. However, a close examination of the results shows that the values of the soilcrete block strengths are not much different from those of sandcrete block strengths. For example, the 50-day strengths are 4.70N/mm² for sandcrete block and 4.30N/mm² for soilcrete block at 100% OPC and 4.55N/mm² for sandcrete block and 4.30N/mm² for soilcrete block at 10% replacement of OPC with RHA-CCA in ternary blending. This also confirms that laterite could be used as sole fine aggregate in making cement composites for low-cost houses in communities where sharp sand is difficult to obtain at affordable prices.

IV. Conclusions

OPC-RHA and OPC-CCA binary blended cement sandcrete and soilcrete blocks as well as OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks have compressive strength values less than those of 100% OPC sandcrete and soilcrete blocks for 5-25% replacement of OPC with pozzolans at 3-28 days of hydration. The blended cement sandcrete and soilcrete block strength values become equal to the control values at about 50 days of curing and greater than the control values beyond 50 days of hydration. Thus, OPC-RHA and OPC-CCA binary blended cements as well as OPC-RHA-CCA ternary blended cement could be used in producing sandcrete and soilcrete blocks with sufficient strength for use in building and minor civil engineering works where the need for high early strength is not a critical factor.

The strength of OPC-RHA binary blended cement sandcrete and soilcrete blocks is consistently greater than that of OPC-CCA binary blended cement specimens for all percentage replacements of OPC with pozzolans at all curing ages. The strength values of OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks were consistently in-between the values of OPC-RHA and OPC-CCA binary blended cement sandcrete and soilcrete blocks. This suggests that more RHA should be used than CCA if the two pozzolans were to be used in unequal proportions to optimize the strength of the OPC-RHA-CCA ternary blended cement sandcrete and soilcrete blocks.

Moreover, the closeness in strength values of OPC-RHA and OPC-CCA binary blended cement sandcrete blocks (this closeness was also observed for soilcrete blocks) and the fact that the strength of the OPC-RHA-CCA ternary blended cement sandcrete blocks was in-between these values suggests that the two agricultural by-product pozzolans could be combined in any available proportions individually in binary blending or together in ternary blending with OPC in making blended cement sandcrete and soilcrete blocks for use in various Nigerian communities.

The strength values of soilcrete blocks were found to be less than those of sandcrete blocks for all percentages of OPC replacement with pozzolans and at all curing ages. Therefore, sand should be used in preference to laterite for making cement blocks. However, since the soilcrete block strengths were not much less than the equivalent sandcrete block strengths, good quality laterite could still be used for block making in the various communities where sand is scarce and unaffordable to the rural populace.

References

- [1] Agbede, I. O., & Obam, S. O. (2008). Compressive Strength of Rice Husk Ash-Cement Sandcrete Blocks. *Global Journal of Engineering Research*, Vol. 7 (1), pp. 43-46.
- [2] Apata, A. O. And Alhassan, A. Y. (2012). Evaluating Locally Available Materials as Partial Replacement for Cement. *Journal of Emerging Trends in Engineering and Applied Sciences (JETEAS)*, 3 (4): 725-728.
- [3] Aribisala, O. J. and Bamisaye, A. J. (2006). Viability of Bone Powder (BP) As Partial Replacement for Cement in Concrete. *Botswana Journal of Technology*, 15 (1): 22-26.
- [4] Baiden, B. K. and Tuuli, M. M. (2004). Impact of quality control practices in sandcrete blocks production. *Journal of Architectural Engineering*, 10 (2): 53-60.
- [5] Cisse, I. K., & Laquerbe, M. (2000). Mechanical characterization of sandcretes with rice husk ash additions: study applied to Senegal. *Cement and Concrete Research*, 30 (1): 13- 18.
- [6] Cordeiro, G. C., Filho, R. D. T., & Fairbairn, E. D. R. (2009). Use of ultrafine saw dust ash with high-carbon content as pozzolan in high performance concrete. *Materials and Structures*, 42: 983-992. DOI 10.1617/s11527-008-9437-z.
- [7] Elinwa, A. U., Ejeh, S. P., & Akpabio, I. O. (2005). Using metakaolin to improve sawdust-ash concrete. *Concrete International*, 27 (11), 49 - 52.
- [8] Fadzil, A. M., Azmi, M. J. M., Hisyam, A. B. B., & Azizi, M. A. K. (2008). Engineering Properties of Ternary Blended Cement Containing Rice Husk Ash and Fly Ash as Partial Cement Replacement Materials. *ICCBT*, A (10): 125 - 134.

- [9] Fri'as, M., Villar-Cocinã, E., Sa'ñchez-de-Rojas, M. I., & Valencia-Morales, E. (2005). The effect that different pozzolanic activity methods has on the kinetic constants of the pozzolanic reaction in sugar cane straw-clay ash/lime systems: Application of a kinetic-diffusive model. *Cement and Concrete Research*, 35: 2137 – 2142.
- [10] Ganesan, K., Rajagopal, K., and Thangavel, K. (2008). Rice husk ash blended cement: assessment of optimal level of replacement for strength and permeability properties of concrete. *Constr. Build. Mater*, 22 (8):1675-1683.
- [11] Habeeb, G. A., &Fayyadh, M. M. (2009).Saw dust ash Concrete: the Effect of SDA Average Particle Size on Mechanical Properties and Drying Shrinkage.*Australian Journal of Basic and Applied Sciences*, 3(3): 1616-1622.
- [12] Joshua, O. and Lawal, P. O. (2011). Cost Optimization of Sandcrete Blocks through Partial Replacement of Sandwith Lateritic Soil.*Epistemics in Science, Engineering and Technology*, 1 (3): 89-94.
- [13] Mama, B.O. and Osadebe, N.N. (2011).Mathematical Model for the Optimization of Compressive Strength of LaterizedSandcrete Blocks. *Nigerian Journal of Technology*, 30(2): 80-86.
- [14] Manasseh, J. (2010). A Review of Partial Replacement of Cement with Some Agro Wastes.*Nigerian Journal of Technology*, 29 (2): 12-20.
- [15] Marthong, C. (2012). Sawdust Ash (SDA) as Partial Replacement of Cement. *International Journal of Engineering Research and Applications(IJERA)*, 2(4): 1980-1985.
- [16] Mehta, P. K. &Pirtz, D. (2000). Use of rice husk ash to reduce temperature in high strength mass concrete. *ACI Journal Proceedings*, 75:60-63.
- [17] Nair, D. G., Jagadish, K. S., and Fraaij, A. (2006). Reactive pozzolanas from rice husk ash: An alternative to cement for rural housing. *CemConcr. Res.*, 36 (6): 1062-1071.
- [18] Okpala, D. C. (1993) Some Engineering Properties of Sandcrete Blocks Containing Rice Husk Ash.*Journal of Building and Environment*, 28 (3): 235-241.
- [19] Oyekan, G. L. and Kamiyo, O. M. (2011).A study on the engineering properties of sandcreteblocks produced with rice husk ash blended cement. *Journal of Engineering and Technology Research*, 3(3): 88-98.
- [20] Rukzon, S., &Chindapasirt, P. (2006). Strength of ternary blended cement mortar containing Portland cement, rice husk ash and fly ash.*J. Eng. Inst. Thailand*, 17: 33-38 (547-551).
- [21] Rukzon, S., Chindapasirt, P., &Mahachai, R. (2009).Effect of grinding on chemical and physical properties of saw dust ash. *International Journal of Minerals, Metallurgy and Materials*, 16 (2): 242-247.
- [22] Sakr, K. (2006). Effects of Silica Fume and Rice Husk Ash on the Properties of Heavy Weight Concrete.*Journal of Materials in Civil Engineering*, 18(3): 367-376.
- [23] Tyagher, S. T., Utsev, J. T., and Adagba, T. (2011). Suitability of Sawdust Ash-Lime Mixture for Production of Sandcrete Hollow Blocks.*Nigerian Journal of Technology*, 30 (1): 79-84.
- [24] Wada, I., Kawano, T., &Mokotomaeda, N. (2000).Strength properties of concrete incorporating highly reactive rice-husk ash. *Transaction of Japan Concrete Institute*, 21 (1): p. 57–62.
- [25] Wenapere, D. A. and Ephraim, M. E. (2009).Physico-mechanical behaviour of sandcrete block masonry units. *Journal of Building Appraisal* 4: 301–309. doi:10.1057/jba.2009.8